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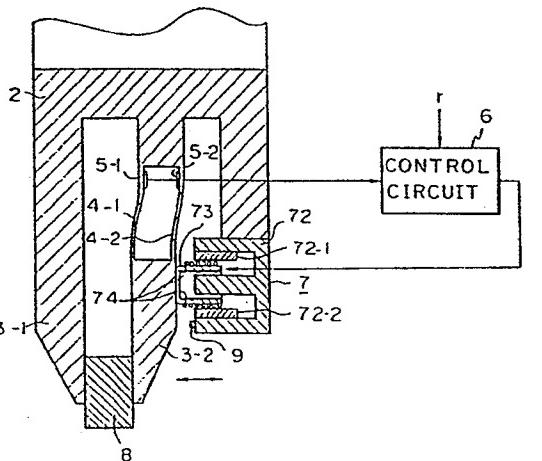
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### (54) Force controlling system.

(57) In a force controlling system, a movable member (3-2) fixed to a resilient member (4-1,4-2) applies a force to an object (8) in correspondence with a force information signal from a control circuit (6). At the same time, an additional force is applied via driving means (7) to the movable member by positive feedback of the displacement of the resilient member to the driving means, so that the reactive force due to the displacement of the resilient member is counteracted by the additional force. As a result, the movable member applies to the object only a force in correspondence to the force information signal. The driving means may be a voice-coil motor. The movable member, the resilient member, the driving means and a fixed finger (3-1) form gripping means, which may be located on the end of a robot arm.

Fig. 1



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FORCE CONTROLLING SYSTEM

This invention relates to a system for controlling a force, and particularly a very small force. Such system  
5 may be used in a gripping apparatus of, for example, a robot or a tactile apparatus.

Recently, remarkable progress in factory automation (FA) or flexible manufacturing systems (FMS) has caused considerable integration of robots into the manufacturing processes.  
10 However, since conventional position control type robots operate regardless of their environment, such robots cannot be applied, for example, to semiconductor processes requiring fine construction operations, to assembling processes for magnetic heads, or to inspection processes for soft food or soft materials. There is  
15 therefore a demand for a system for controlling a very small force in robots, free of the above disadvantages.

For example, in the prior art, in the case of control of a gripping force, a pressure sensor is  
20 provided in a gripping portion of a hand, thereby controlling the gripping force at an open angle of the hand. In this case, it is necessary to switch between a position control mode and a force control mode at a certain timing. However, it is difficult to control such  
25 a timing. In addition, since the difference in gain between the position control mode and the force control mode is affected by the speed of motion of the hand, vibration and collision occur at the timing when the hand comes into contact with an object. Hence, it is almost  
30 impossible to control a gripping force within a small range. Furthermore, a control circuit and a sensor are required for each of the position control mode and the force control mode, thus increasing the manufacturing cost.

It is an object of the present invention to provide a system for controlling a force, in particular, a very small force, and a gripping apparatus, such as a robot, including such system.

5 Embodiments of the invention will now be described, by way of example, with reference to the accompanying drawings, wherein:

Figure 1 is a cross-sectional view of a robot hand according to a first embodiment of the invention;

10 Figure 2 is a control block diagram of the robot hand of Figure 1;

Figure 3 is a circuit diagram of a control circuit of Figure 1;

15 Figure 4 is an exploded perspective view of another robot hand for use in the invention;

Figure 5 is an exploded, perspective view for explaining the assembly of the robot hand of Figure 4;

Figure 6 is a perspective view of a robot hand according to a second embodiment of the invention;

20 Figure 7 is a perspective view of a robot hand according to a third embodiment of the invention;

Figure 8 is a perspective view of a modification of the robot hand of Figure 7;

25 Figures 9 and 10 are control system block diagrams for explaining the operation of the robot hand of Figures 7 and 8;

Figure 11 is an elevational view of another modification of the robot hand of Figure 7;

30 Figure 12 is a side view of the robot hand of Figure 11;

Figure 13 is a cross-sectional view taken along a line A-A' of Figure 11;

Figure 14 is an elevational view of a robot hand similar to Figure 11;

Figure 15 is a side view of the robot hand of Figure 14;

Figures 16A and 16B are diagrams of another modification of part of the robot hand of Figure 7;

5 Figure 17 is an elevational view of a further modification of the robot hand of Figure 7;

Figure 18 is a cross-sectional view of a feed screw of Figure 17;

10 Figure 19 is an elevational view of a robot hand according to a fourth embodiment of the invention;

Figure 20 is a perspective view of a tactile apparatus according to a fifth embodiment of the invention;

15 Figures 21 and 22 are cross-sectional views of the apparatus of Figure 20;

Figure 23 is a block diagram of a control system for explaining the operation of the apparatus of Figure 20;

20 Figure 24 is a perspective view of a robot system according to a sixth embodiment of the present invention; and

Figure 25 is a partly broken perspective view of two-dimensional force generating apparatus of Figure 24.

In Fig. 1, which illustrates a first embodiment of the present invention, reference numeral 1 designates a robot arm on which a hand base 2 is mounted. The hand base 2 has two finger portions 3-1 and 3-2. In this case, the finger portion 3-1 is a rigid member, i.e., a stationary member, while the finger portion 3-2 is supported by two parallel-plate springs 4-1 and 4-2 which are linked between the portion 3-2 and the hand base 2. That is, the finger portion 3-2 serves as a movable member. Each of the parallel-plate springs 4-1 and 4-2 generates reactive force when the finger portion 3-2 is shifted, as indicated by arrows, from a balance point. Fixed to the inside of the parallel-plate springs 4-1 and 4-2 are strain gauges 5-1 and 5-2, respectively, for detecting the displacement of the parallel-plate springs 4-1 and 4-2. The output signals of the strain gauges 5-1 and 5-2 are supplied to a control circuit 6 which receives a force information signal  $\gamma$ .

The control circuit 6 controls a voice coil motor 7 which is a kind of linear motor. The voice coil motor 7 is composed of a yoke 72 having permanent magnets 72-1 and 72-2, and a bobbin 73 on which a coil 74 is wound. The yoke 72 is fixed to the hand base 2, while the bobbin 73 is fixed to the finger portion 3-2.

Thus, the control circuit 6 controls the voice coil motor 7 to drive the finger portion 3-2, thereby gripping an object 8 with the two finger portions 3-1 and 3-2. Reference numeral 9 designates a stop.

Note that the parallel-plate springs 4-1 and 4-2 have low shear moduli in one direction and high shear moduli in other directions, and accordingly, the parallel-plate springs 4-1 and 4-2 serve as a one way guide.

In Fig. 1, the gripping force of the finger portions 3-1 and 3-2 is controlled by the force generated by the voice coil motor 7, not by the opening angle of the

finger portions 3-1 and 3-2. In addition, the output signals of the strain gauges 5-1 and 5-2 are fed back positively to the voice coil motor 7 via the control circuit 6.

- 5      The control block diagram of the robot hand of Fig. 1/illustrated in Fig. 2. In Fig. 2, reference S designates a Laplace operator,  $O_c$  designates an open-loop gain of the power amplifier (not shown) of the control circuit 6, B designates a space magnetic flux density of the voice coil motor 7, and  $\ell$  designates the number of turns of the coil 74. Therefore,  $B\ell$  is the force constant of the voice coil motor 7. The output  $V_1(S)$  of the power amplifier of the control circuit 6 is applied positively to the coil 74, and in addition,
- 10     15 the counterelectromotive force  $V_2(S)$  of the voice coil motor 7 obtained by multiplying the displacement speed  $X(S)$  by the force constant  $B\ell$  is applied negatively to the coil 74. That is,  $V(S) (=V_1(S)-V_2(S))$  is applied to the coil 74.
- 20     25 The current  $I(S)$  flowing through the coil 74 is obtained by dividing  $V(S)$  by the impedance  $(LS+R)$  of the voice coil motor 7, where L and R are the inductance and resistance thereof, respectively. The force  $F_1(S)$  generated by the voice coil motor 7 is obtained by multiplying the current  $I(S)$  by the force constant  $B\ell$  of the voice coil motor 7. This force  $F_1(S)$  is applied positively to the movable portion, i.e., the finger portion 3-2. Also, the reactive force  $F_2(S)$  of the parallel-plate springs 4-1 and 4-2, which is  $kX(S)$  ( $k$ : spring constant of the springs 4-1 and 4-2,  $X(S)$ : displacement of the finger portion 3-2), is applied negatively to the finger portion 3-2. That is, the force  $F(S) (= F_1(S)-F_2(S))$  is applied to the finger portion 3-2.
- 30     35 The displacement speed  $X(S)$  is obtained by dividing  $F(S)$  by the mechanical impedance  $(MS+D)$  of the finger portion 3-2, where M and D are the mass and damping

coefficient thereof, respectively.

Note that the force  $F_1(S)$  generated by the voice coil motor 7 has a good linear characteristic regarding the current  $I(S)$ , since the space magnetic flux density  $B$  of the voice coil motor 7 is definite. As a result, the calculated force is substantially consistent with the measurement thereof.

In the control circuit 6 of Fig. 2, although the displacement  $X(S)$  of the finger portion 3-2 and a force information signal  $R(S)$  are fed back positively to the voice coil motor 7, while the displacement speed  $\dot{X}(S)$  of the finger portion 3-2 and the current of the voice coil motor 7 are fed back negatively to the voice coil motor 7, here,  $P_c$ ,  $V_c$ , and  $I_c$  are feedback gains of the displacement  $X(S)$ , the displacement speed  $\dot{X}(S)$ , and the current  $I(S)$ , respectively.

The characteristics of the voice coil motor 7 are represented by

$$e = R_i + L \frac{di}{dt} + B_i \dot{x} \quad \dots (1)$$

$$B_i i = M \ddot{x} + D \dot{x} + kx \quad \dots (2)$$

In addition, the transfer function of the force information signal  $R(S)$  to the displacement  $X(S)$  of the finger portion 3-2 is represented by

$$\frac{X(S)}{R(S)} = 1 / \left\{ \frac{LM}{B_i} S^3 + \frac{1}{B_i} (M I_c O_c + RM + LD) S^2 + \right.$$

$$\left. \left( \frac{I_c D}{B_i} + V_c \right) O_c + B_i + \frac{kL + RD}{B_i} \right\} S +$$

$$\left( \frac{kI}{B_i} - P_c \right) O_c + \frac{kR}{B_i} \quad \dots (3)$$

Therefore, the damping coefficient of the entire system is represented by

$$\left( \frac{I_c D}{B_i} + V_c \right) O_c + B_i + \frac{kL + RD}{B_i} \quad \dots (4)$$

Also the stiffness of the entire system is represented

by

$$\left( \frac{kI_c}{Bl} - P_c \right) O_c + \frac{kR}{Bl} \quad \dots (5)$$

- Therefore, where the force information signal R(S) is changed in step, the steady-state position error of the displacement X(S) is

$$\lim_{S \rightarrow 0} S X(S) = \frac{1}{\left( \frac{kI_c}{Bl} - P_c \right) O_c + \frac{kR}{Bl}} \quad \dots (6)$$

- Since the gain  $O_c$  of the power amplifier is generally very large, for example from 80 dB to 100 dB, and  $\frac{kR}{Bl}$  is nearly zero, the steady-state position error is nearly zero. This is preferable for position control-type robots, but is not preferable for force control.
- type robots because, if the width of an object is not accurate, the voice coil motor 7 serves as a spring having a spring constant as shown in formula (6) due to the error of a width indication value, thereby generating a large force within a low frequency band. Thus, it is impossible to control a force such as a gripping force.

- In the present invention, the gain  $P_c$  of the position error is as low as possible while retaining the entire system in a stable state, thereby preventing a force due to the position error from being generated.
- This is possible, since the displacement  $X(S)$  is fed back "positively" to the voice coil motor 7, that is, the sign of the gain  $P_c$  is negative in the formula (6). In other words, in the present invention

$$P_c \approx \frac{k}{Bl} \left( \frac{R}{O_c} + I_c \right) \approx \frac{kI_c}{Bl} \quad \dots (7)$$

- In this state, as is apparent from the formula (3), the spring constant of the parallel-plate springs 4-1 and 4-2 seems to be very small, for example, experimentally 0.1 g/mm. Therefore, if the stroke of the finger portions 3-1 and 3-2 is  $\pm 2$  mm, the maximum generated force is  $\pm 0.2$  g.

Note that the gain  $V_c$  of the displacement speed  $\dot{X}(S)$  and the gain  $I_c$  of the current  $I(S)$  are determined appropriately by using the formulas (4) and (5).

Thus, if a positive gripping force component is given as  $R(S)$ , the robot hand of Fig. 1 can grip the object 8 with a gripping force within an error of  $\pm 0.2$  g, regardless of the width of the object 8. Conversely, if a negative gripping force is given as  $R(S)$ , the finger portions 3-1 and 3-2 are opened, and accordingly, the finger portion 3-2 comes in contact with the stopper 9 with a definite force.

Also, in Fig. 1, it is possible to measure the width of the object 8 by using the output signals of the strain gauges 5-1 and 5-2.

An example of the control circuit 6 of Fig. 1 is illustrated in Fig. 3. In Fig. 3, the output signals of the strain gauges 5-1 and 5-2 are supplied to a buffer 31. The output signal of the buffer 31 is supplied to a buffer 32 having the gain  $P_c$  and a differentiator 33 having the gain  $V_c$ . Reference numeral 34 designates a resistor for detecting the current flowing through the voice coil motor 7. The current detecting means formed by the resistor 34 has the gain  $I_c$ . Reference numeral 35 is a power amplifier having the open gain  $O_c$ . The force information signal  $r(R(S))$  and the output  $\{\dot{X}(S)\}$  of the buffer 32 are applied positively to the power amplifier 35, while the output  $\{\dot{X}(S)\}$  of the differentiator 33 and the output  $\{I(S)\}$  of the resistor 34 are applied negatively to the power amplifier 35. The output of the power amplifier 35 is applied to output transistors 36 and 37. That is, the power amplifier 35 drives the voice coil motor 7 via the output transistors 36 and 37, so that the sum of  $R(S) + \dot{X}(S) - I(S)$  is zero.

In Fig. 2, the gains  $P_c$ ,  $V_c$ , and  $I_c$  are manually adjusted. However, if the control circuit 6 is incorporated into a microcomputer, these gains  $P_c$ ,  $V_c$ , and  $I_c$

can be adjusted by software.

In Fig. 1, since the voice coil motor 7 of a cylinder type is provided on the outside of the finger portion 3-2, the robot hand becomes relatively large.

- 5 Contrary to this, in Fig. 4, which is a modification of the robot hand of Fig. 1, a voice coil motor 7' of a plate type is provided on the side of the finger portions 3-1 and 3-2, thereby reducing the size of the robot hand. The voice coil motor 7' of a plate type is composed of
- 10 two yokes 71'-1 and 71'-2, permanent magnets 72'-1 and 72'-2, a coil 73' of a plate type having terminals 73'a, a bobbin 74', and a spacer 75' of a non-magnetic material. Reference numerals 10 and 11 designate screw holes for assembling the voice coil motor 7'.
- 15 The yoke 71'-1 having the permanent magnet 72'-1, the spacer 75', and the yoke 71'-2 having the permanent magnet 72'-2 are mounted on the hand base 2 by inserting screws into the screw holes 11. On the other hand, the plate type coil 73' associated with the bobbin 74' is
- 20 mounted on the finger portion 3-2 by inserting screws into the screw holes 10. Thus, when a current is supplied to the plate-type coil 73' via the terminals 73'a, the current flowing through the coil 73' interacts with a magnetic circuit formed by the permanent magnets 72'-1
- 25 and 72'-2, thereby moving the finger portion 3-2.

Note that such a voice coil motor 7' can be provided on both sides of the finger portions 3-1 and 3-2.

- The bobbin 74' of Fig. 4 is conventionally made of plastic such as a resin. However, since plastic has a
- 30 low heat conductivity, a plastic bobbin may be distorted by the heat generated by the coil 73'. Therefore, it is preferable that the bobbin 7' be made of aluminium, since aluminium has a high heat conductivity, a high shear modulus, and a high electrical conductivity. When
  - 35 an aluminium bobbin of a high electrical conductivity moves within a magnetic field, a large eddy current is generated in the bobbin, thereby increasing the damping

coefficient of the voice coil motor 7', which is helpful in stabilizing the entire control system. In this case, it is necessary to completely insulate the coil 73' from the aluminium bobbin 74'. For this purpose, the aluminium bobbin 74' is preferably made by alumite processing, thereby obtaining a high insulation regardless of the number of turns of the coil 73'. Further, it is preferable that the aluminium bobbin 74' be made by black alumite processing, thereby avoiding flaws in the coil 73'. Still further, a groove having the same configuration as the coil 73' is formed in the bobbin 74'.

Cobalt magnets having high magnetic susceptibility are used as the permanent magnets 72'-1 and 72'-2, to reduce the size thereof. However, since a strong magnetic attraction or repulsion is generated between such magnetized cobalt magnets, some problems occur when mounting the magnetized cobalt magnets on the yokes.

In order to easily mount the magnetized cobalt magnets 72'-1 and 72'-2 on the yokes 71'-1 and 71'-2, respectively, a magnet fixing frame 76' of non-magnetic material is provided for each of the magnets 72'-1 and 72'-2, as illustrated in Fig. 5. That is, apertures 76'a and 76'b are provided in the magnet fixing frame 76', and accordingly, the mounting of the magnets 72'-2, 72'-1 is carried out by inserting the magnets into the apertures 76'a and 76'b. The thickness of the magnet fixing frame 76' is equal to or a little smaller than that of the magnets 72'-2, 72'-1.

The robot hands as illustrated in Figs. 1 through 5 can grip an object having a small range of width depending upon the length of the parallel-plate type springs 4-1 and 4-2. For example, such a width range is about 4 mm. Therefore, exchange of the robot hands is carried out in accordance with the magnitude of width of the objects.

In Fig. 6, which illustrates a second embodiment of the present invention, the finger portions 3-1 and 3-2

- are provided at a feed screw 61 which is divided into a left-handed screw portion and a right-handed screw portion. For example, the finger portion 3-1 is provided at the left-handed screw portion, while the finger  
5 portion 3-2 is provided at the right-handed screw portion. Therefore, if the feed screw 61 rotates in one direction, the finger portion 3-1 approaches the finger portion 3-2, while, if the feed screw 61 rotates in the other direction, the finger portion 3-1 separates from  
10 the finger portion 3-2. That is, the span between the finger portions 3-1 and 3-2 is controlled by the rotation of the feed screw 61 which is driven by a direct current (DC) motor 62. The DC motor 62 is connected to an angle encoder 63.
- 15 The finger portion 3-2 is also supported by the parallel-plate springs 4-1 and 4-2 (see Figs. 1 and 4) and is driven by the voice coil motor 7' which is the same as that of Fig. 4. Therefore, the voice coil motor 7' is controlled by the control circuit 6 which is the  
20 same as that of Fig. 1.

As explained above, the span between the finger portions 3-1 and 3-2 is driven by the DC motor 62. This DC motor 62 is controlled by another control circuit 64 which is composed of a constant current amplifier 641.  
25 That is, in the control circuit 64, a span information signal sp is applied positively to the amplifier 641, while the output of the angle encoder 63 is applied negatively to the amplifier 641. Therefore, the DC motor 62 is controlled by the negative feedback of the  
30 angle encoder 63 to the DC motor 62, so that the output of the encoder 63 coincides with the span information signal sp.

Thus, the voice coil motor 7' is used for the control of a gripping force and the DC motor 62 is used  
35 for the control of the span between the finger portions 3-1 and 3-2, thereby controlling a gripping force for an object regardless of the width thereof.

If a gripping force is controlled by only the DC motor with no voice coil motor, it is almost impossible to control a very small gripping force of the order of grams, since a blind band exists in a control system due 5 to the friction of the movable portions such as the feed screw 61 and the DC motor 62. Of course, in the embodiment of Fig. 6, it is also impossible to counteract the span error due to the above-mentioned blind band. However, it is possible to control a fine gripping force 10 by driving the voice coil motor where the span error is, for example,  $\pm 2$  mm.

In other words, in the robot hand of Fig. 6, if the span information signal  $sp$  having an accuracy of  $\pm 2$  mm is given to the control circuit 64, it is possible to 15 grip an object with a fine gripping force, since the voice coil motor 7' has no friction portion.

Note that the control circuits 6 and 64 can be also incorporated into a microcomputer, so that the parameters such as  $\gamma$ ,  $sp$  and the like are controlled by software.

20 In Fig. 6, the output of the displacement sensor (in this case, the strain gauges) is fed back to the control circuit 6, thereby controlling the voice coil motor 7', while the output of the angle encoder 63 is fed back to the control circuit 64, thereby controlling 25 the DC motor 62. That is, the control for a gripping force is independent of the control for a span between the finger portions.

In Fig. 7, which illustrates a third embodiment of 30 the present invention, there is illustrated a robot hand similar to the robot hand of Fig. 6. However, the robot hand of Fig. 7 comprises no angle encoder. In Fig. 7, the output of the strain gauges (not shown) is applied positively to the control circuit 6, thereby controlling the voice coil motor 7' which is the same as that of 35 Fig. 4, and the output of the strain gauges is also applied negatively to a control circuit 6', thereby controlling the DC motor 62. That is, the output of the

strain gauges is applied to both of the control circuits 6 and 6'.

In Fig. 8, which is a modification of the robot hand of Fig. 7, the voice coil motor 7 of Fig. 1 is used 5 instead of the voice coil motor 7' of Fig. 4. The robot hand of Fig. 8 has the same control means as that of Fig. 7. Note that reference numeral 81 is a stopper.

In the robot hand of Fig. 7 (or Fig. 8), the voice coil motor 7' (or 7) mounted on the finger portion 3-2 10 is mainly operated, while the DC motor 62 for rotating the feed screw 61 is additionally operated. That is, when it is impossible to grip an object by only the operation of the voice coil motor 7' (or 7), the DC motor 62 is rotated so as to obtain a predetermined span 15 between the finger portions 3-1 and 3-2.

Note that it is also impossible to control a small gripping force only by controlling the DC motor 62 in the same way as in the second embodiment of Fig. 6.

The control block diagrams of the robot hand of 20 Fig. 7 (or Fig. 8) are illustrated in Figs. 9 and 10. The control block diagram of Fig. 9 shows the state where the finger portion 3-2 is not in contact with an object, while the control block diagram of Fig. 10 shows the state where the finger portion 3-2 is in contact 25 with the object.

That is, as is understood from Figs. 9 and 10, in the embodiment of Fig. 7, the output of the strain gauges 5-1 and 5-2 fixed to the parallel-plate springs 4-1 and 4-2 (see: Fig. 1) is fed back positively to the 30 voice coil motor 7', and simultaneously, the above-mentioned output is fed back negatively to the DC motor 62. In other words, the feed control of the feed screw 61 and the gripping force of the finger portions 3-1 and 3-2 are both controlled by detecting the 35 placement of the parallel-plate springs 4-1 and 4-2.

Referring to Fig. 9, the difference voltage  $V(S)$  between the output voltage  $V_1(S)$  of the power amplifier

of the control circuit 6 and the counterelectromotive force  $V_2(S)$  is applied to the coil 73' (or 73) of the voice coil motor 7' (or 7). Therefore, the current  $I(S)$  flowing through the coil 73' (or 73) is given by

$$I(S) = \frac{V(S)}{L_c S + R_c}$$

where  $L_c$  and  $R_c$  are the inductance and resistance of the voice coil motor 7' (or 7) and  $L_c S + R_c$  is the impedance of the voice coil motor 7' (or 7). The force

- 10  $F_1(S)$  generated by the voice coil motor 7' (or 7), which is  $B_l I(S)$  ( $B_l$ : force constant and current of the voice coil motor 7' (or 7), is applied positively to the finger portion 3-2, while the reactive force  $F_2(S)$  of the parallel-plate springs 4-1 and 4-2, which is  $kX(S)$  ( $k$ : spring constant of the springs 4-1 and 4-2,  $X(S)$ : displacement of the finger portion 3-2), is applied negatively to the finger portion 3-2. Also, applied negatively to the finger portion 3-2 is a force  $F_3(S)$  given by

$$F_3(S) = M_c S \cdot \dot{X}(S)$$

- where  $M_c$  is the mass of the finger portion 3-2 and  $\dot{X}(S)$  is the displacement speed of the feed screw 61. That is, the force  $F(S)$  ( $=F_1(S)-F_2(S)-F_3(S)$ ) is applied 25 to the finger portion 3-2. Therefore, the displacement speed  $\dot{X}(S)$  of the finger portion 3-2 is given by

$$\dot{X}(S) = \frac{F(S)}{M_c S}$$

- Also, the displacement  $X(S)$  of the finger portion 30 3-2 is given by  $X(S) = \frac{\dot{X}(S)}{S}$ .

The control circuit 6 of Fig. 9 has the same configuration as the control circuit 6 of Fig. 2, except that the force information signal is given by  $U_2(S)$ .

- On the other hand, the difference voltage  $V'(S)$  35 between the output voltage  $V_1'(S)$  of the power amplifier of the control circuit 6' and the counterelectromotive force  $V_2'(S)$  is applied to the DC motor 62. Therefore,

the current  $I'(S)$  flowing through the DC motor 62 is given by

$$I'(S) = \frac{V'(S)}{L_m S + R_m}$$

5 where  $L_m$  and  $R_m$  are the inductance and resistance of the DC motor 62 and  $L_m S + R_m$  is the impedance of the DC motor 62. The force  $F_1'(S)$  generated by the DC motor 62, which is  $K_m I'(S)$  ( $K_m$ ,  $I'(S)$ : induced voltage constant and current of the DC motor 62), is applied positively to the feed screw 61, while the frictional force  $F_r(S)$  of the DC motor 62, the feed screw 61, and the like is applied negatively to the feed screw 61. Also, applied negatively to the feed screw 61 is a force  $F_3'(S)$  given by

$$F_3'(S) = M_c S \dot{X}'(S)$$

where  $M_c$  is the mass of the finger portion 3-2 and  $X(S)$  is the displacement speed of the finger portion 3-2. That is, the force  $F'(S)$  ( $=F_1'(S)-F_r(S)-F_3'(S)$ ) is applied to the feed screw 61. Therefore, the displacement speed  $\dot{X}'(S)$  of the feed screw 61 is given by

$$\dot{X}'(S) = \frac{F'(S)}{(M_m + M_c)S}$$

25 where  $M_m$  is the mass obtained by subtracting the mass of the movable portion of the voice coil motor 7' (or 7) from the load mass of the DC motor 62.

Note that damping coefficients are omitted from the mechanical impedance terms of Figs. 9 and 10.

In the control circuit 6',  $P_m$ ,  $V_m$ , and  $I_m$  are feedback gains of the displacement, the displacement speed, and current of the feed screw 61, respectively. In addition,  $O_m$  is an open-loop gain of the power amplifier of the control circuit 6'. Here, a span information signal  $U_1(S) (=0)$  is given to the power amplifier. An actual circuit of the control circuit 6' can be constructed in the same manner as in Fig. 3, and accordingly, the details thereof are omitted.

In the state as illustrated in Fig. 9, the dynamic equations thereof are as follows.

$$M_c \ddot{x}_c + (M_m + M_c) \ddot{x}_m = -D_m \dot{x}_m + K_m I_m - F_r \dots (8)$$

$$M_c (\ddot{x}_m + \ddot{x}_c) = -kx_c - D_c \dot{x}_c + B_l I_c \dots (9)$$

$$L_m \dot{I}_m = -R_m I_m + E_m - K_m \dot{x}_m \dots (10)$$

$$L_c \dot{I}_c = -R_c I_c + E_c - B_l x_c \dots (11)$$

Here,  $x_c$  is the displacement of the finger portion 3-2;

$x_m$  is the displacement of the feed screw 61;

$E_c$  is the voltage of the voice coil motor 7' (or 7); and

$E_m$  is the voltage of the DC motor 62.

In the state as illustrated in Fig. 9, the force information signal  $U_2(S)$  is given to the voice coil motor 7' (or 7), and the span information signal  $U_1(S)$  ( $= 0$ ) is given to the DC motor 62. As a result, the voice coil motor 7' (or 7) moves the finger portion 3-2 at a definite position defined by the stopper 81, and accordingly,  $x_c$  is generated in the displacement of the finger portion 3-2. Therefore, the DC motor 62 is operated by the control circuit 6' so as to reduce the displacement  $x_c(X(S))$  of the finger portion 3-2. In this case, however, even when the DC motor 62 is operated, the displacement  $x_c$  cannot be zero, unless the acceleration of the DC motor 62 is very large.

Finally, the finger portion 3-2 touches an object, and as a result, the dynamic equations (8), (9), (10), and (11) are changed as follows.

$$M_m \ddot{x}_c = -kx_c + B_l I_c + K_m I_m - F_r - (D_m + D_c) \dot{x}_c \dots (12)$$

$$L_m \dot{I}_m = -R_m I_m + E_m - K_m \dot{x}_c \dots (13)$$

$$L_c \dot{I}_c = -R_c I_c + E_c - B_l x_c \dots (14)$$

That is, if a timing when the finger portion 3-2 touches the object is an initial value ( $t = 0$ ), the control system is as illustrated in Fig. 10. Here, assuming that the open-loop gains  $O_m$  and  $O_c$  of the power amplifiers are

$$O_m = O_c = \infty.$$

Then, the transfer function of the entire system is represented by

$$\begin{aligned} & \frac{K_m}{I_m} U_1(s) + \frac{K_c}{I_c} U_2(s) \\ &= \left( M_m s^2 + \left( \frac{K_m}{I_m} V_m + \frac{K_c}{I_c} V_c \right) s + \frac{K_m p_m}{I_m} - \frac{K_c p_c}{I_c} + k \right) X(s) \\ &+ F_r(s) \end{aligned} \quad \dots (15)$$

- 10 Since  $U_1(s) = 0$ , the input  $U_2(s)$ , the frictional force  $F_r(s)$ , and the output  $X(s)$  satisfy the following equation.

$$\begin{aligned} (X(s)) &= \frac{K_c}{I_c} \cdot \frac{1}{M_m s^2 + \left( \frac{K_m}{I_m} V_m + \frac{K_c}{I_c} V_c \right) s + \frac{K_m p_m}{I_m} - \frac{K_c p_c}{I_c} + k} \cdot U_2(s) \\ &- \frac{1}{M_m s^2 + \left( \frac{K_m}{I_m} V_m + \frac{K_c}{I_c} V_c \right) s + \frac{K_m p_m}{I_m} - \frac{K_c p_c}{I_c} + k} \cdot F_r(s) \end{aligned} \quad \dots (16)$$

Thus, from the equation (16), it can be seen that:

- i) the entire control system is observable and controllable if

$$\frac{K_m}{I_m} p_m - \frac{K_e}{I_e} p_e + k > 0;$$

- ii) a steady-state position error is generated for a step input response;  
 iii) a steady-state position error is generated due to the frictional force; and  
 iv) two actuators, i.e., the voice coil motor 7' (or 7) and the DC motor 62 are controllable as one hybrid motor.

- That is, since the characteristics as stated in i) to iv) are the same as those of a system having only one DC motor, no improvement occurs for position control. However, the gripping force  $F(s)$  for the finger portion

3-2 is represented by

$$F(S) = \frac{K_c}{I_c} U_2(S) - \frac{K_c}{I_c} (V_c S - P_c + \frac{I_c}{K_c} k) X(S) \dots (17)$$

5 Therefore, if the displacement feedback gain  $P_c$  is set by

$$P_c = \frac{I_c}{K_c} k \dots (18)$$

and the displacement speed feedback gain  $V_c$  is zero, then

$$F(S) = \frac{K_c}{I_c} U_2(S) \dots (19)$$

That is, the gripping force  $F(S)$  is controllable regardless of the displacement  $X(S)$ , and is also controllable without a time delay and a steady-state position error.

- 15 In other words, after the finger portion 3-2 touches the object, it is possible to accurately control a fine gripping force regardless of the steady-state position error of the DC motor 62.

Note that, even when the displacement speed feedback gain  $V_c$  is zero, the damping coefficient of the entire system is not zero due to the damping coefficient  $D_c$ , which is, however, very small, so that the system is stable.

In order to satisfy the equation (18), a linear relationship between the spring constant  $k$  of the parallel-plate springs 4-1 and 4-2 and the output of the displacement sensor is necessary. Since the parallel-plate springs 4-1 and 4-2 have a small shear modulus in one direction, and accordingly, are not subjected to torsion, the strain gauges 5-1 and 5-2 as the displacement sensor can accurately detect the spring constant  $k$  of the springs 4-1 and 4-2.

Thus, in the third embodiment, it is possible to accurately control a force including a large force and a very small force, regardless of external disturbances such as friction. Also, since an object is gripped under the condition that the displacement of the springs

is nearly zero, the feed screw 61 and the female screw portion of the finger portions 3-1 and 3-2 do not rub together, thereby improving the endurance thereof.

As is apparent from the equations (16) and (18),  
5 the response speed of the robot hand of Fig. 7 (or  
Fig. 8) is dependent upon the position feedback gain  
 $P_m$  of the DC motor 62. The control system is generally  
unstable, i.e., in an oscillating state when the gain  
 $P_m$  is large, however, such an oscillating state can be  
10 suppressed by the frictional force  $F_r(S)$ . Therefore,  
in the third embodiment, since the gripping force of the  
robot hand is not affected by the position error due to  
the frictional force  $F_r(S)$ , the frictional force  $F_r(S)$   
can be moderately large thereby increasing the response  
15 speed. In this regard, since a screw mechanism such as  
the feed screw 61 is used in the robot hand of Fig. 7,  
the motion of the feed screw 61 generates a large  
frictional force thereby increasing the response speed.

Figures 11 through 15 illustrate a modification of  
20 the robot hand of Fig. 7. In more detail, Fig. 12 is a  
side view of the robot hand of Fig. 11, and Fig. 13 is a  
cross-sectional view taken along the line A-A'. Also,  
Figs. 14 and 15 correspond to Figs. 11 and 12, respectively.  
That is, in Figs. 11 and 12, the voice coil  
25 motor 7' is omitted. However, in Figs. 14 and 15, the  
voice coil motor 7' is illustrated. As illustrated in  
Figs. 11 and 14, a protrusion 1101 is provided outside  
of the finger portion 3-2. Therefore, when the feed  
screw 61 is rotated so as to move the finger portion 3-2  
30 towards the outside, the protrusion 1101 is in contact  
with a side plate 1102 provided on a base 1103 of the  
robot hand. Thus, the opening of the robot hand is also  
carried out by a force control mode. That is, in Figs. 9  
and 10, when a negative force information signal is  
35 given as  $U_2(S)$ , the finger portion 3-2 is moved toward  
the outside by the voice coil motor 7' (or 7), so that  
the displacement of the finger portion 3-2 is detected

by the parallel-plate springs 4-1 and 4-2 and is transmitted to the control circuit 6' for controlling the DC motor 62. As a result, the DC motor 62 drives the feed screw 61 to move the finger portion 3-2 towards the outside. Then, when the protrusion 1101 of the finger portion 3-2 is in contact with the side plate 1102, the displacement of the finger portion 3-2 is restored and the displacement of the springs 4-1 and 4-2 is restored, thereby stopping the DC motor 62.

10 In Fig. 16A, which is a modification of the finger portions 3-1 and 3-2 of Fig. 7, finger portins 3-1' and 3-2' are shaped to grip an object such as a cylindrical object 8' as illustrated in Fig. 16B. When gripping such an object 8', a negative force information signal 15 is given as  $U_2(S)$  in Figs. 9 and 10. Note that other modifications are possible for the shape of the finger portions 3-1 and 3-2.

In Fig. 17, which is still another modification of the robot hand of Fig. 7, the finger portions 3-1 and 20 3-2 are mounted on the feed screw 61 by inserting the feed screw 61 into the female screw portions 171-1 and 171-2 of the finger portions 3-1 and 3-2. In addition, the female screw portions 171-1 and 171-2 of the finger portions 3-1 and 3-2 are reinforced by nuts 172-1 25 and 172-2, respectively, and, in this case, elastic elements 173-1 and 173-2, which are made of, for example, rubber, are inserted therebetween. As a result, referring to Fig. 18 which is a partly cross-sectional view of the elastic element 173-2 of Fig. 17, the elastic element 173-2 generates forces as indicated by arrows, thereby avoiding backlash between the female portions 171-1 and 171-2 of the finger portions 3-1 and 3-2 and the feed screw 61. Such a backlashless structure is helpful in adjusting a predetermined frictional force 30  $F_r(S)$ .

In Fig. 19, which is a fourth embodiment of the present invention, an angle encoder 63' and a control

circuit 19 are added to the elements of Fig. 7, in order to measure the width of a gripped object. Note that the control circuits 6 and 6' are omitted from Fig. 19. The control circuit 19 comprises an amplifier 191 for the 5 displacement signal of the strain gauges 5-1 and 5-2, an analog/digital (A/D) converter 192, a central processing unit (CPU) 193, and a counter 194 for counting the output signal of the angle encoder 63'.

The operation of measuring the width of an object 10 is carried out as follows. First, a zero point is set, that is, the finger portions 3-1 and 3-2 are closed with no object therebetween. At this time, the counter 194 is cleared and the displacement signal of the strain gauges is stored as an initial displacement value  $D_0$  15 in the memory (not shown). Then, when actually gripping an object in the same manner as explained above, the CPU193 fetches the displacement signal value D from the strain gauges and the value C of the counter 194, and calculates the width W by

$$W = C + \alpha(D - D_0)$$

where  $\alpha$  is an experimentally determined constant. Thus, the width of an object such as a soft object can be easily measured.

In Fig. 20, which is a fifth embodiment of the 25 present invention, a tactile apparatus is illustrated. Figure 21 is also a cross-sectional view of the tactile apparatus of Fig. 20, and Fig. 22 is an enlarged view of the voice coil motor portion of Fig. 21.

Referring to Figs. 20, 21, and 22, reference 30 numeral 101 designates a contact probe, 102 a voice coil motor, 103 two parallel-plate springs, 104 a stopper, 105 a movable portion of a movable mechanism, 106 a housing, 107 a robot arm, 108 a strain gauge, 109 a feed screw of the movable mechanism, 110 a nut portion of the 35 movable mechanism, 111 and 112 bearings, 113 a DC motor, 114 an angle encoder, 115 a stopper/guide for the nut portion 110, and 116 a control circuit comprising two

control circuits 1161 1162 for controlling the voice coil motor 102 and the DC motor 113, respectively, and a control circuit 1163 for measuring the dimension.

Referring to Fig. 22, the voice coil motor 102 is composed of a yoke 1021, permanent magnets 1022 mounted on the yoke 1021, a movable portion 1023, a coil 1024 wound on the movable portion 1023, and a stopper 1025 for stopping the movable portion 1023.

The contact probe 101 is mounted on the movable portion 1023, and accordingly, the contact probe 101 can come in contact with an object 117 with a predetermined force. The movable portion 1023 of the voice coil motor 102 is supported by the parallel plate springs 103. Therefore, the parallel-plate springs 103 are displaced by the force of the voice coil motor 102 and the reactive force of the contact probe 101. On the other hand, the yoke 1021 of the voice coil motor 102 is mounted on the movable portion 105 of the movable mechanism, and in addition, the base of the parallel-plate springs 103 is mounted on the movable mechanism.

Referring to Figs. 21 and 22, the strain gauge 108 is fixed to the parallel-plate springs 103. Therefore, when the parallel-plate springs 103 are displaced, and a torsion is generated therein, the displacement of the springs 103 is detected by the strain gauge 108 which transmits an output to the control circuit 116. The movable portion of the movable mechanism is connected to the feed screw 109 at the nut portion 110 thereof, and accordingly, the DC motor 113 drives the movable portion 105 with a large stroke. The movable portion 105 is slidably connected via the linear bearing 111 to the stopper/guide 115 fixed to the housing 106. The stopper/guide 115 stops the rotation of the nut portion 110. The rotational angle of the DC motor 113 detected by the angle encoder 114 is in proportion to the motion amount of the movable portion 105 driven by the feed screw 109.

In the same way as in the previously-mentioned

embodiment, the voice coil motor 102 has no frictional mechanism, while the movable mechanism by the DC motor 113, the feed screw 109 and the like is frictional.

In Fig. 20, the control circuit 1161 receives the 5 output signal of the strain gauge 108 to control the voice coil motor 102, while the control circuit 1162 receives the output signal of the strain gauge 108 to control the DC motor 113. That is, the control circuits 1161 and 1162 correspond to the control circuits 6 and 6' 10 of Fig. 7, respectively. Also, the control circuit 1163 is similar to the control circuit 19 of Fig. 19.

The control system of the tactile apparatus of Figs. 20, 21, and 21 is illustrated in Fig. 23 which is the same as Fig. 9, except that analog switches SW1 and 15 SW2 for switching operation modes are provided. The dynamic system of the tactile apparatus of Fig. 23 shows the state wherein the contact probe 101 is not in contact with the object 117. When the contact probe 101 is in contact with the object 117, the dynamic system of 20 the tactile apparatus is replaced by the dynamic system as shown in Fig. 10.

In Fig. 23, a motion indication signal  $U(S)$  is given to only the control circuit 1161. Also, the displacement  $X(S)$  of the voice coil motor 102 is fed 25 back positively thereto, while the displacement  $X(S)$  of the voice coil motor 102 is fed back negatively to the DC motor 113. That is, if the state of the analog switches SW1 and SW2 is as illustrated in Fig. 23, the operation of the tactile apparatus of Fig. 20 is the 30 same as that of the robot hand of Fig. 7.

The method for measuring a three-dimensional shape will be explained

1) Set of Initial Contact Pressure

The force due to the movable portion 1023 of 35 the voice coil motor 102 applied to the parallel-plate spring 103 is dependent upon the attitude of the voice coil motor 102. Therefore, every time the attitude of

the voice coil motor 102 is changed, it is necessary to change the initial contact pressure. That is, after the attitude of the contact probe 1 is set, the analog switches SW1 and SW2 are switched so that the displacement  $X(S)$  of the voice coil motor 102 is fed back negatively thereto, and the feedback amount of the displacement  $X(S)$  to the DC motor 113 is zero. As a result, when the parallel-plate springs 103 are held in a neutral state in which the current  $I(S)$  flowing through the coil 1024 of the voice coil motor 102 generates a force in balance with the weight of the voice coil motor 102, such a current  $I(S)$  is stored as the initial contact pressure in the memory (not shown) by the control circuit 1163. Thus, the initial pressure value is added to a pressure indication value, thereby obtaining a predetermined contact pressure.

2) Set of Initial Dimension

In this case, the analog switches SW1 and SW2 are switched to a measuring mode. That is, the state of the analog switches SW1 and SW2 is the same as illustrated in Fig. 23. As a result, the displacement  $X(S)$  of the voice coil motor 102 is fed back positively thereto, and the displacement  $X(S)$  of the voice coil motor 102 is applied positively to the DC motor 113. When the control circuit 1163 detects that the housing 106 is pressing on the stopper 104 at a definite pressure, the control circuit 1163 clears the counter (see Fig. 19) and stores the displacement of the voice coil motor 102 as the initial dimension in the memory.

30 3) Measurement

After completion of the steps 1) and 2), it is possible to measure an object unless the attitude of the voice coil motor 102 is changed. That is, the measured dimension is determined by the sum or difference of the motion amount of the feed screw 109 and the displacement of the parallel-plate springs 103.

According to the tactile apparatus as shown in

Figs. 20, 21, and 22, it is possible to support the contact probe 1 with a very small force of the order of grams. Also, since the set position of the contact probe is not strictly fixed, it is easy to carry out an initial set, thereby enabling automation of the dimension measurements. Further, even if an object is relatively soft, it is possible to measure the dimension of the object without damaging it.

The above-mentioned force generating apparatus, the gripping apparatus, or the tactile apparatus can be individually used and be incorporated into a robot system. Note that the force generating apparatus corresponds to the gripping apparatus having only one finger portion, such as 3-2.

A robot system incorporating a force generating apparatus is illustrated in Fig. 24. In Fig. 24, reference numeral 201 designates a robot base having an X-axis driving motor, 202 an arm having a Z-axis driving motor, 203 an arm having a Y-axis driving motor, 204 a hand, 205 a two-dimensional force generating apparatus having two kinds of voice coil motors, and 206 a control circuit. The control circuit 206 is comprised of an operation panel 2061, a memory 2062, a CPU 2063, a hand position control circuit 2064, a hand position detector circuit 2065, a driver circuit 2066, and a hand control circuit 2067. During a position control mode, the position control circuit 2064 receives position indication signals from the CPU 2063, thereby controlling the driver circuit 2066 for driving the robot base 201 and the arms 202 and 203. However, during a force control mode, the position indication signals from the CPU 2063 regarding the X- and Y-axis are zero, so that the position control circuit 2064 controls the driver circuit 2066 by receiving the displacement  $X(S)$  and  $Y(S)$  of the voice coil motors included in the force generating apparatus 205. In this case, the displacement  $X(S)$  regarding the X-axis is fed back positively to the voice

coil motor regarding to the X-axis. However, the displacement  $X(S)$  is fed back negatively to the X-axis driving motor. Similarly, the displacement  $Y(S)$  regarding the Y-axis is fed back positively to the voice coil 5 motor regarding to the Y-axis, whilst the displacement  $Y(S)$  is fed back negatively to the Y-axis driving motor.

Referring to Fig. 25, which is a detailed diagram 10 of the two-dimensional force generating apparatus of Fig. 24, reference numerals 2051 and 2052 designate bases fixed to the arm 203 and the hand 206, respectively, 4X and 4Y plate-type springs in the X- and Y-directions, respectively, 5X and 5Y strain gauges in the X- and Y-directions, respectively, 72X and 72Y permanent magnets, and 74X and 74Y coils in the X- and Y-directions, respectively. In this case, the permanent 15 magnets 72X and the coil 74X form an X-direction voice coil motor, and the permanent magnets 72Y and the coil 74Y form a Y-direction voice coil motor.

In the embodiment of Fig. 24, a two-dimensional 20 force generating apparatus is used. However, it is possible to use a three-dimensional force generating apparatus having three voice coil motors.

Further, when the tactile apparatus according to 25 the present invention is incorporated into a robot system, the absolute coordinates of an object can be recognized easily by adding the coordinates of the robot arm to the value from the angle encoder of the DC motor of the tactile apparatus.

CLAIMS

1. A force generating apparatus for applying a force to an object in response to a force information signal, characterised by a base member (2); a resilient member (4-1,4-2) fixed to the base member; a movable member (3-2), fixed to the resilient member, for applying the force corresponding to the force information signal to the object; detecting means (5-1,5-2), provided in the resilient member, for detecting the displacement thereof; driving means (7) for driving the movable member; and control means (6), connected to the detecting means and to the driving means for controlling the driving means by positive feedback of the displacement of the resilient member thereto, so as to counteract the reactive force due to the displacement of the resilient member applied to the object, whereby the movable member substantially applies only the force corresponding to the force information signal to the object.
2. Gripping apparatus for gripping an object, including force generating apparatus as claimed in claim 1, characterised by finger means, incorporating the base member (2), the resilient member (4-1,4-2), the movable member (3-2), the detecting means (5-1,5-2), and the driving means (7).
3. Tactile apparatus, characterised by a base member (105); a resilient member (103) fixed to the base member; a movable member (1023) fixed to the resilient member; a contact probe (101) mounted on the movable member, for applying a force corresponding to predetermined force information to an object; detecting means (108) provided in the resilient member, for detecting displacement thereof; driving means (102) for driving the movable member; control means, connected to the detecting means and to the driving means, for controlling the driving means by positive feedback of the

displacement of the resilient member thereto, so as to counteract the reactive force due to the displacement of the resilient member applied to the object, whereby the movable member substantially applies only the force  
5 corresponding to the force information signal to the object; and measuring means, connected to the detecting means, for measuring the shape of the object by the output of the detecting means.

4. Apparatus as claimed in any preceding claim,  
10 characterised in that the driving means comprises a linear motor (7,102).

5. Apparatus as claimed in any preceding claim, characterised in that the driving means comprises a voice coil motor (7,102).

15 6. Object processing apparatus, characterised by a movable mechanism (61); force generating apparatus mounted on the movable mechanism, and comprising a base member, a resilient member (4-1,4-2) fixed to the base member, a movable member (3-2), fixed to the resilient member, for applying a force corresponding to a force information signal to an object; detecting means (5-1,5-2), provided in the resilient member, for detecting the displacement thereof; and first driving means (7') for driving said movable member; the  
20 apparatus being further characterised by first control means (6), connected to the detecting means and to the first driving means, for controlling the first driving means by positive feedback of the displacement of the resilient member thereto, so as to counteract the  
25 reactive force due to the displacement of the resilient member applied to the object, whereby the movable member substantially applies only the force corresponding to the force information signal to the object; second driving means (62) for driving the movable mechanism; and second  
30

control means (64) for controlling the second driving means.

7. Apparatus as claimed in claim 6, characterised by second detecting means (63) connected to the second driving means (62), for detecting the displacement of the movable mechanism (61), the second control means receiving a position indication signal and a position detecting signal from the second detecting means to control the second driving means so that the position detecting signal coincides with the position indication signal.

8. Apparatus as claimed in claim 6, characterised in that the second control means (64) is connected to the detecting means to control the second driving means (62) by negative feedback of the displacement of the resilient member thereto.

9. Apparatus as claimed in any one of claims 6-8, characterised in that the movable mechanism is an arm of a robot.

10. Apparatus as claimed in claim 6 or claim 9, characterised by gripping apparatus having finger means mounted on the movable mechanism and incorporating the base member; the resilient member (4-1,4-2); the movable member (3-2); the detecting means (5-1,5-2); and the first driving means (7').

11. Robot apparatus, characterised by an arm (10); a tactile apparatus mounted on the end of said arm, the tactile apparatus comprising a base element (105), a resilient member (103) fixed to the base member, a movable member (1023) fixed to the resilient member; first driving means (102) for driving the movable member, a contact probe (101), mounted on the movable element, for applying to an object a force corresponding to predetermined force information, and first detecting means (108), provided in the resilient member, for detecting the displacement thereof; the apparatus

- further comprising first control means (1161), connected to the first detecting means and the first driving means, for controlling the first driving means by positive feedback of the displacement of the resilient member thereto, so as to counteract the reactive force due to the displacement of the resilient member applied to the object, whereby the movable member substantially applies to the object only the force corresponding to the force information signal; second driving means (113) for driving the arm; and second control means (1162), connected to the second driving means and to the first detecting means for controlling the second driving means by negative feedback of the displacement of the resilient member thereto; second detecting means (114), connected to the second driving means, for detecting the displacement of the movable member; and measuring means (1163), connected to the first and second detecting means, for measuring the shape of the object from the outputs of the first and second detecting means.
- 20 12. Apparatus as claimed in any one of claims 6-11, characterised in that the movable mechanism comprises a feed screw (61) mounting the force generating apparatus thereon.
- 25 13. Apparatus as claimed in claim 12, characterised in that the movable mechanism further comprises a nut (172-1,172-2) mounted on the feed screw (61), for adjusting the force generating apparatus.
- 30 14. Apparatus as claimed in claim 13, characterised in that the movable mechanism further comprises a resilient antibacklash member (173-1,173-2) inserted between the force generating apparatus (171-1,171-2) and the nut.
- 35 15. Apparatus as claimed in claim 12, characterised in that the feed screw (61) has a left-hand screw portion and a right-hand screw portion, on one of which portions

is mounted the movable member (171-2) and on the other of which portions is mounted finger means.

16. Apparatus as claimed in claim 15, characterised in that the movable mechanism further comprises two nuts 5 (172-1,172-2) mounted on the feed screw (61) for adjusting the movable member and the finger means.

17. Apparatus as claimed in claim 16, characterised in that the movable mechanism further comprises two resilient members (173-1,173-2) inserted between the 10 movable member and the finger means and the respective nut (172-1,172-2).

18. Apparatus as claimed in any one of claims 6-17, characterised in that the second driving means (62) comprises a DC motor.

15 19. Apparatus as claimed in any one of claims 6-18, characterised in that the first driving means (7,102) comprises a linear motor.

20 20. Apparatus as claimed in any one of claims 6-18), characterised in that the first driving means (7,102) comprises a voice coil motor.

21. Apparatus as claimed in claim 5 or claim 20, characterised in that the voice coil motor (7) comprises a plate-type coil (73'), and at least two plate-type permanent magnets (71,72) sandwiching the coil.

25 22. Apparatus as claimed in claim 21, characterised in that the permanent magnets (71,72) are cobalt magnets.

23. Apparatus as claimed in claim 21 or claim 22, characterised in that the voice coil motor (7') further comprises a bobbin (74') of aluminium.

30 24. Apparatus as claimed in claim 23, characterised in that the bobbin of aluminium (74') is made by alumite processing.

25. Apparatus as claimed in any one of claims 35 21-24, characterised in that the voice coil motor (7') further comprises a non-magnetic plate (76') having

apertures (76'a,76'b) for receiving the plate-type permanent magnets (72-2).

26. Apparatus as claimed in any preceding claim, characterised in that the force generating apparatus is  
5 two-dimensional.

27. Apparatus as claimed in any one of claims 1-25, characterised in that the force generating apparatus is three-dimensional.

28. Apparatus as claimed in any preceding claim,  
10 characterised in that the resilient member (4-1,4-2;103) comprises leaf spring means.

29. Apparatus as claimed in any one of claims 1-27, characterised in that the resilient member comprises parallel-plate springs.

15 30. Apparatus as claimed in any preceding claim characterised in that the detecting means (5-1,5-2;108) comprises strain gauge means.

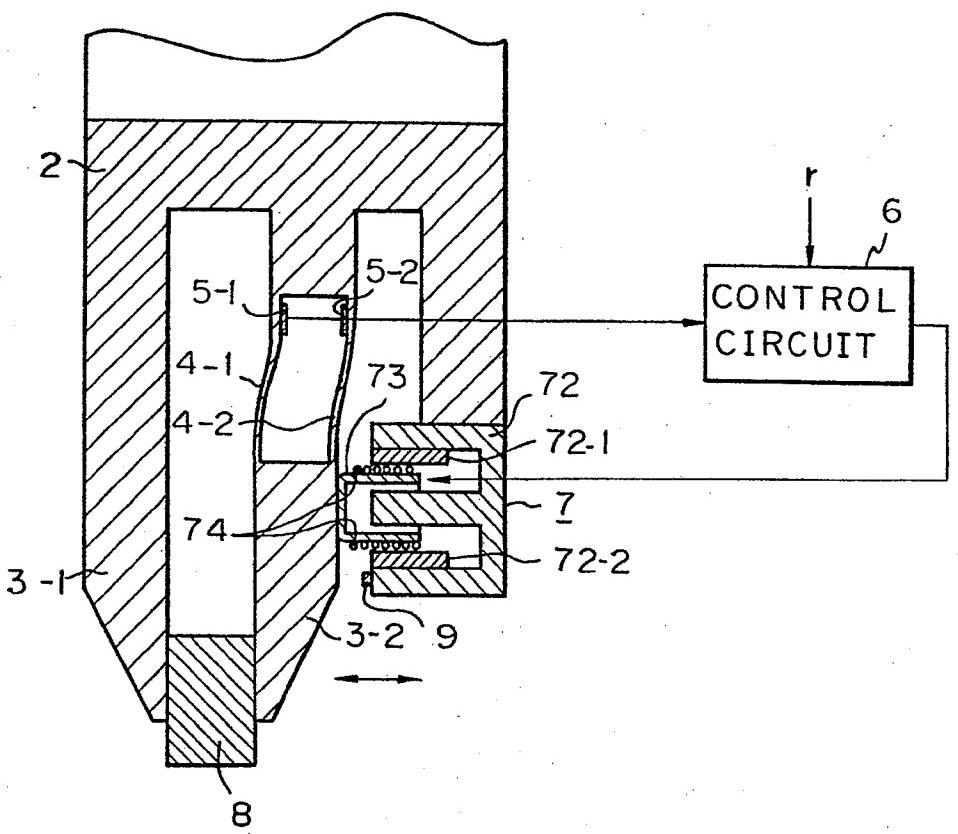
31. Apparatus as claimed in claim 3, characterised by a movable mechanism (110) for moving the base member  
20 (105); further driving means (113) for driving the movable mechanism; and further control means (1162), connected to the further driving means and to the detecting means, for controlling the further driving means by negative feedback of the displacement of the  
25 resilient member (103) thereto.

32. Apparatus as claimed in claim 31, characterised by further detecting means (114), connected to the further driving means (113), for detecting the displacement of the movable mechanism, the measuring  
30 means being connected to the further detecting means to measure the shape of the object by the outputs of the detecting means and the further detecting means.

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Fig. 1



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Fig. 2

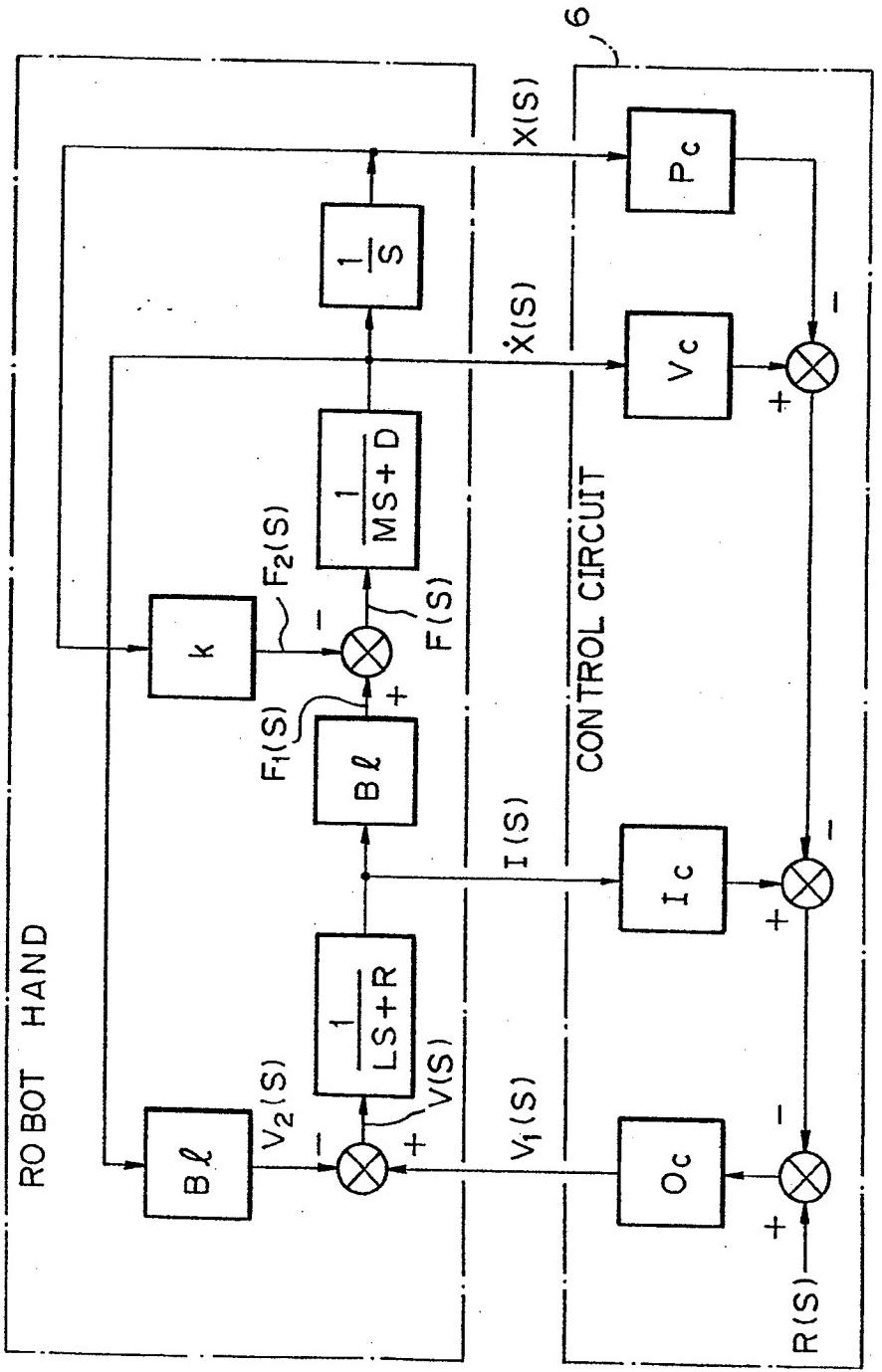
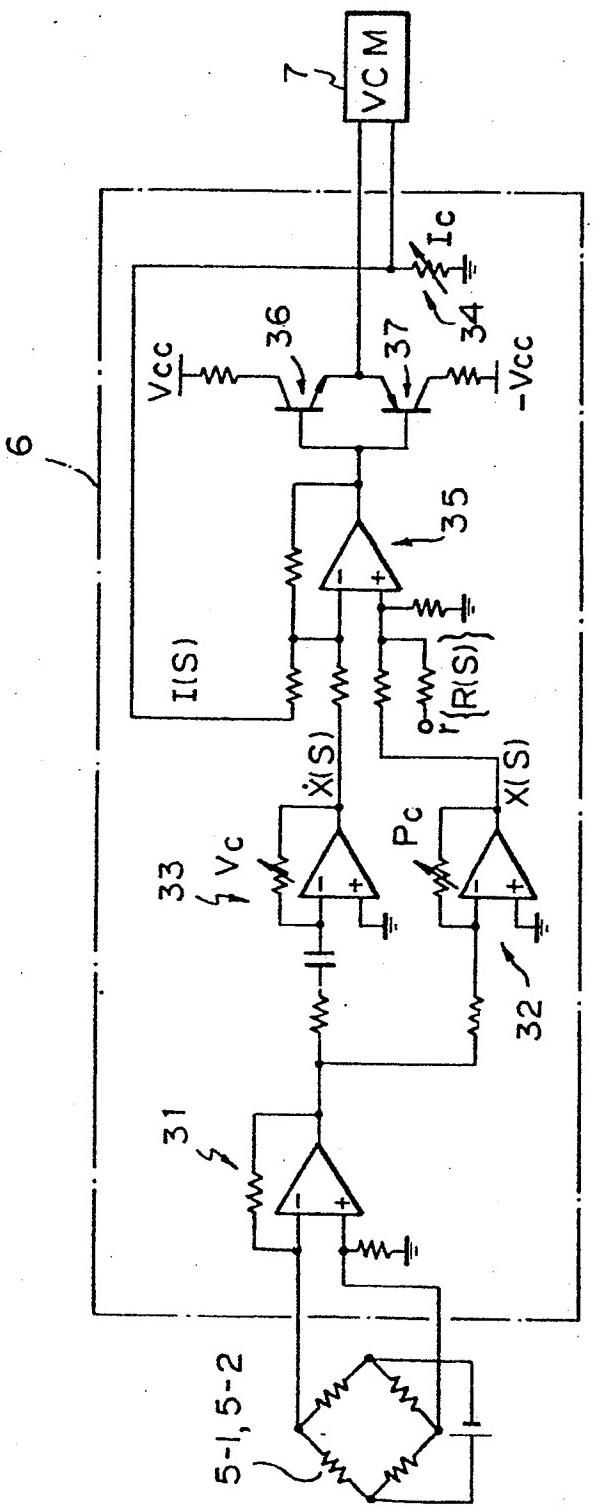


Fig. 3



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Fig. 4

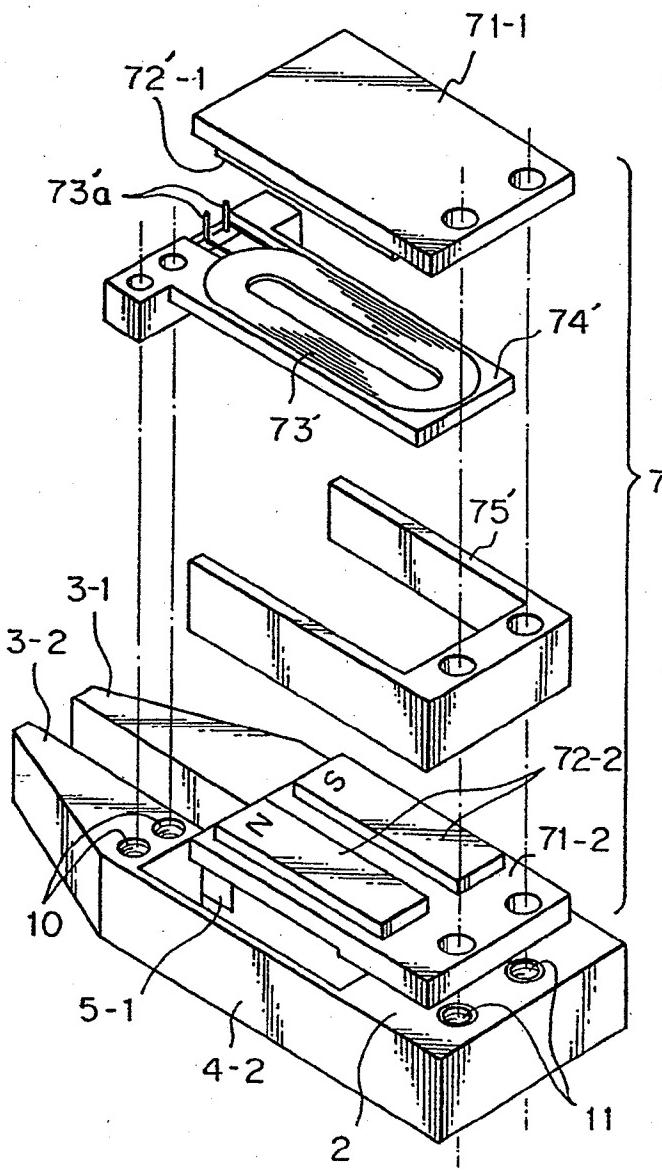
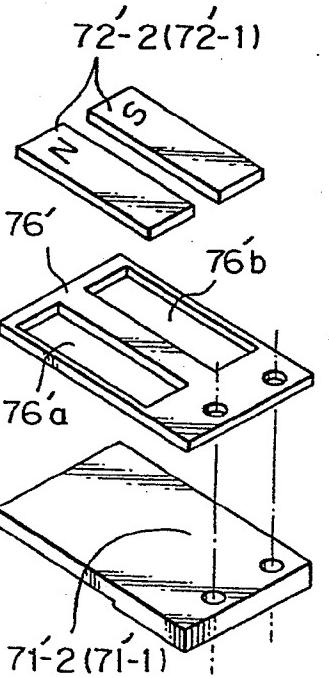


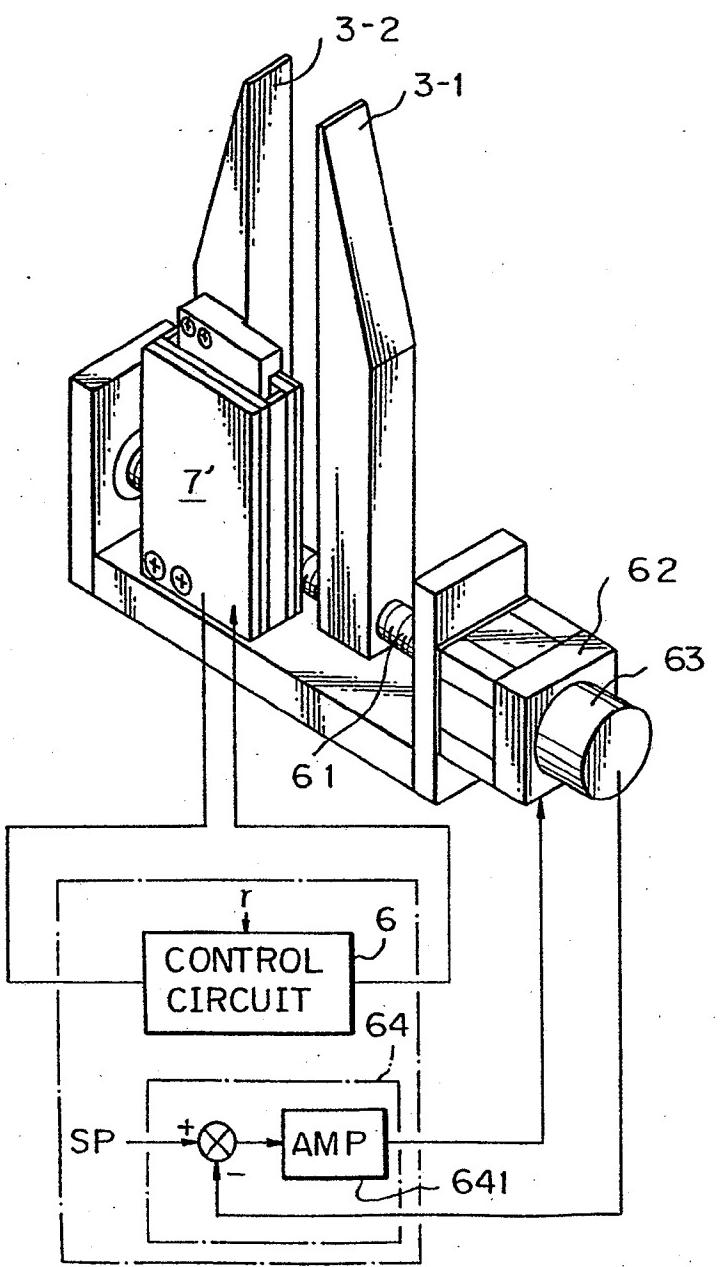
Fig. 5



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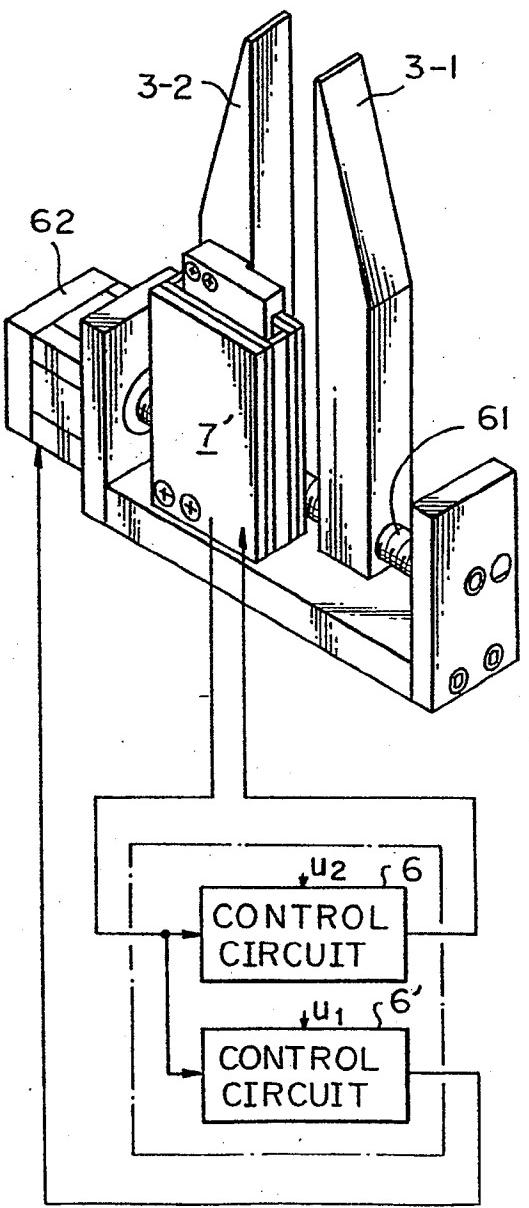
Fig. 6



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Fig. 7



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Fig. 8

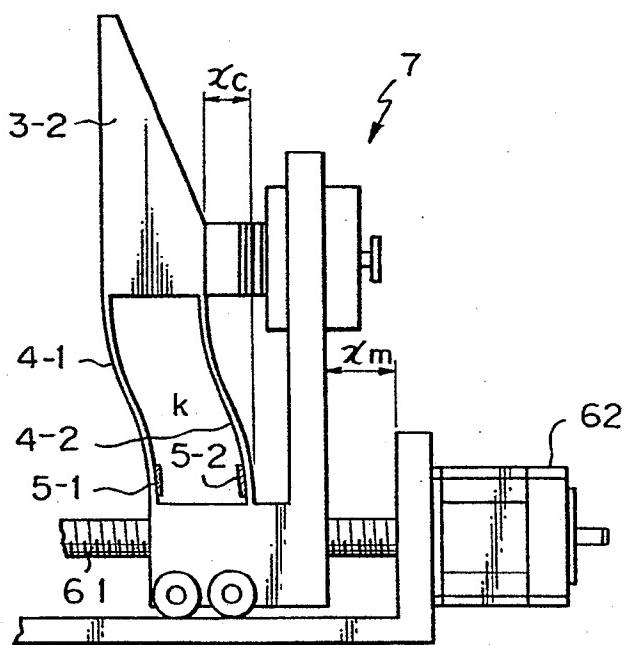
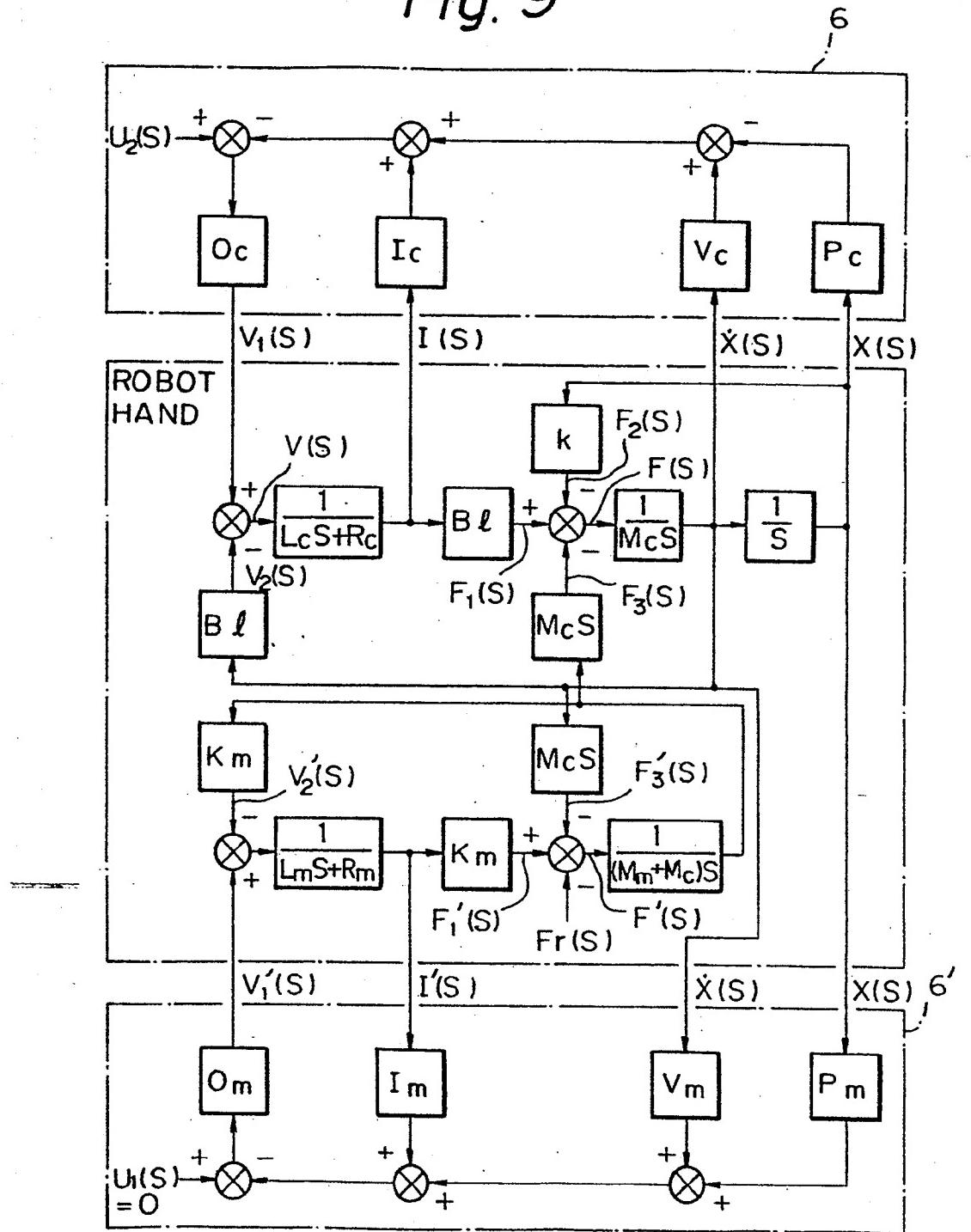


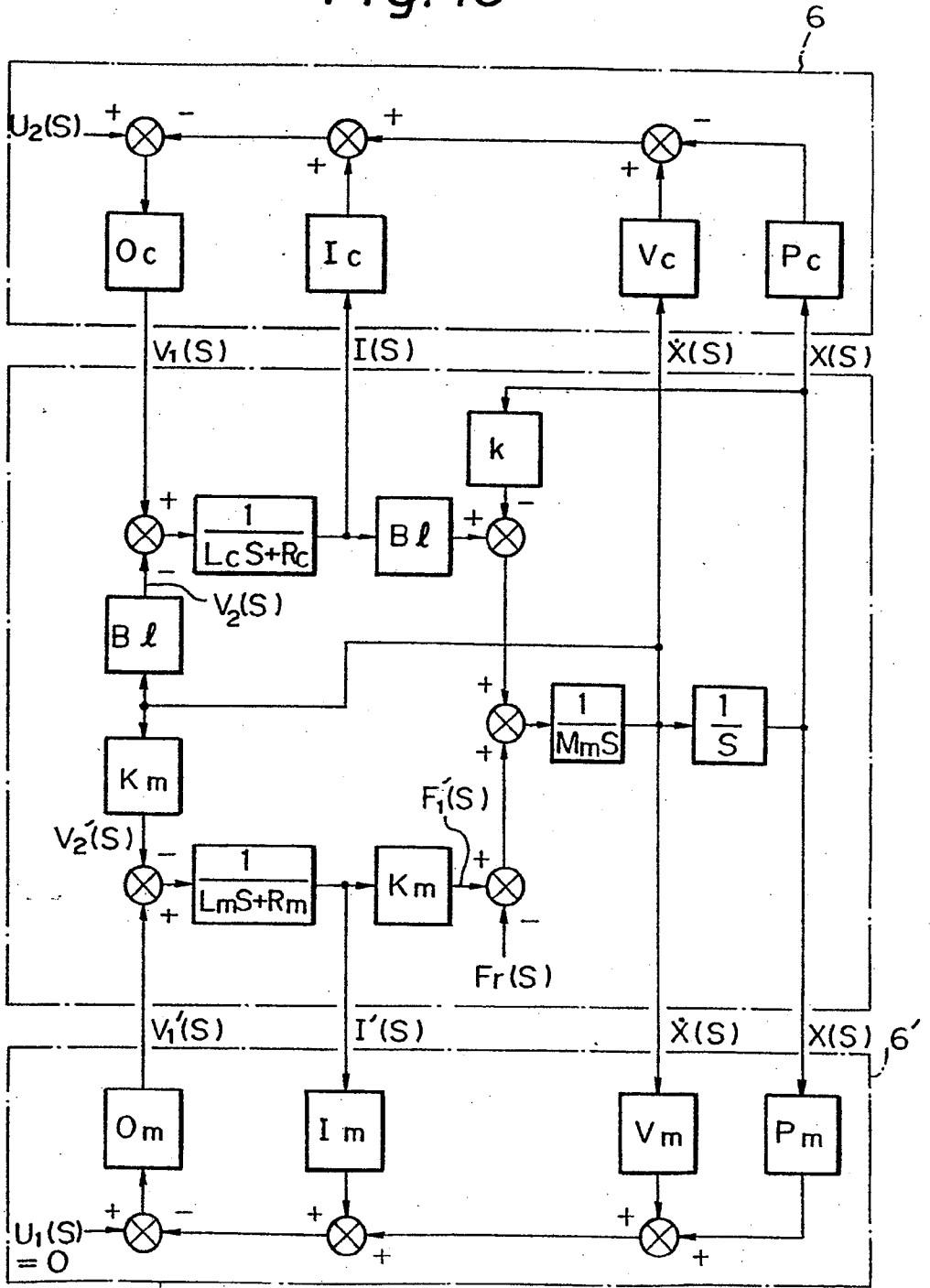
Fig. 9



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*Fig. 10*



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Fig. 11

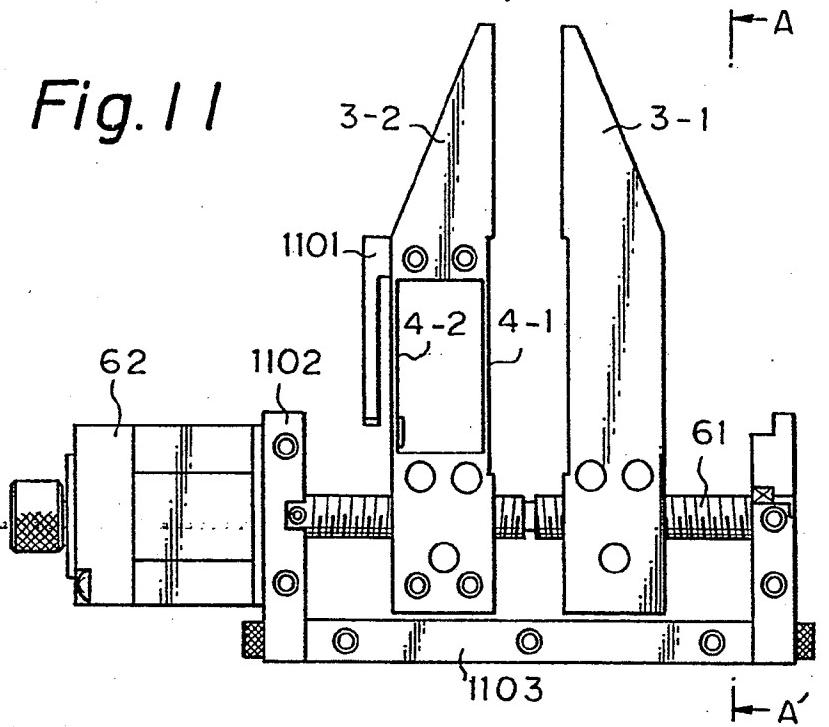


Fig. 12

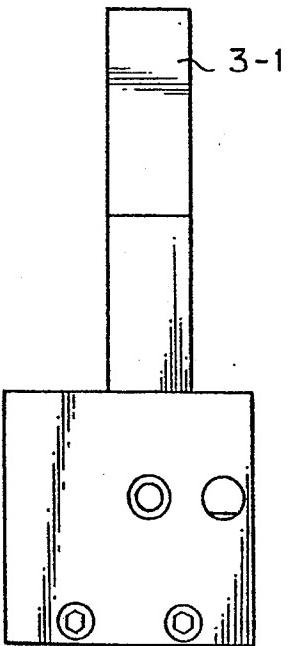
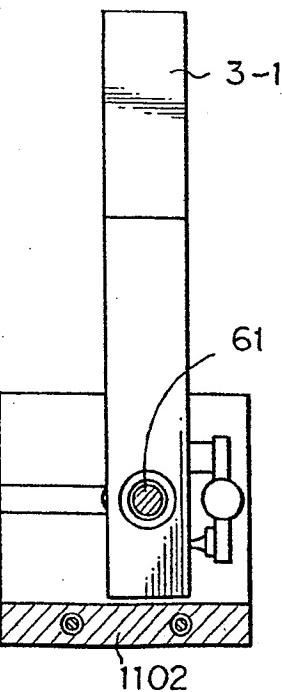


Fig. 13



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Fig. 14

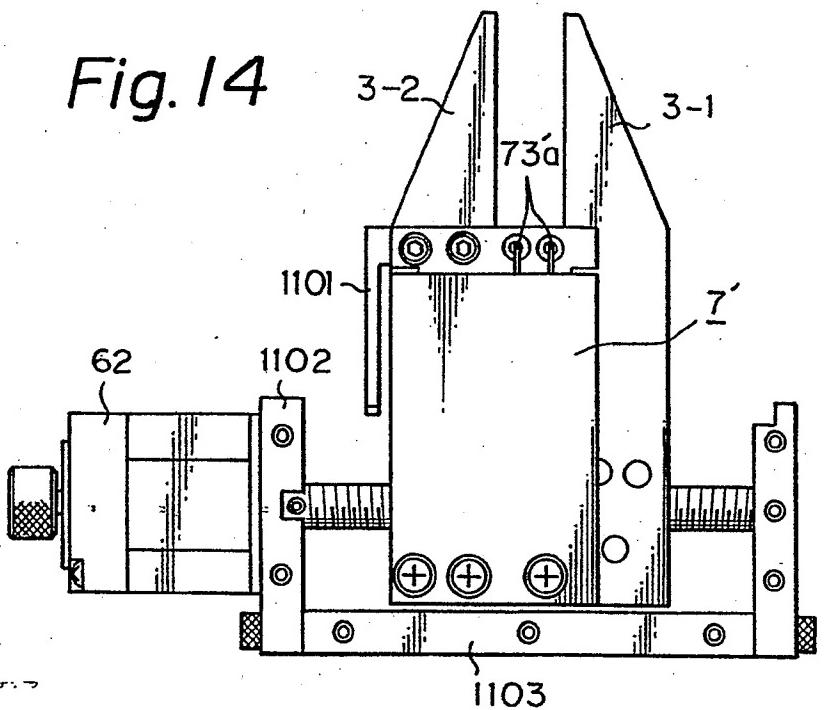


Fig. 15

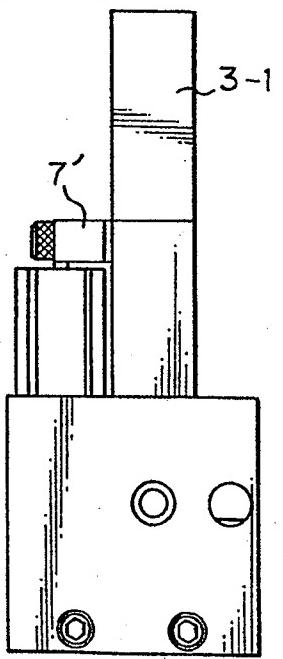


Fig. 16A

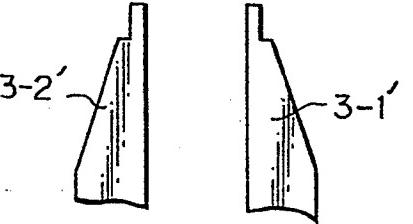
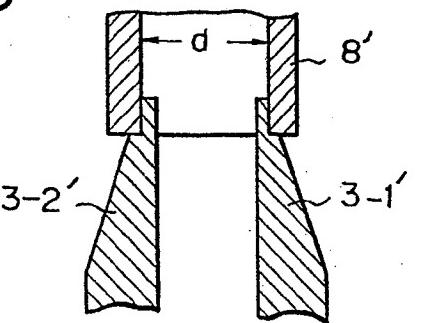


Fig. 16B



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Fig. 17

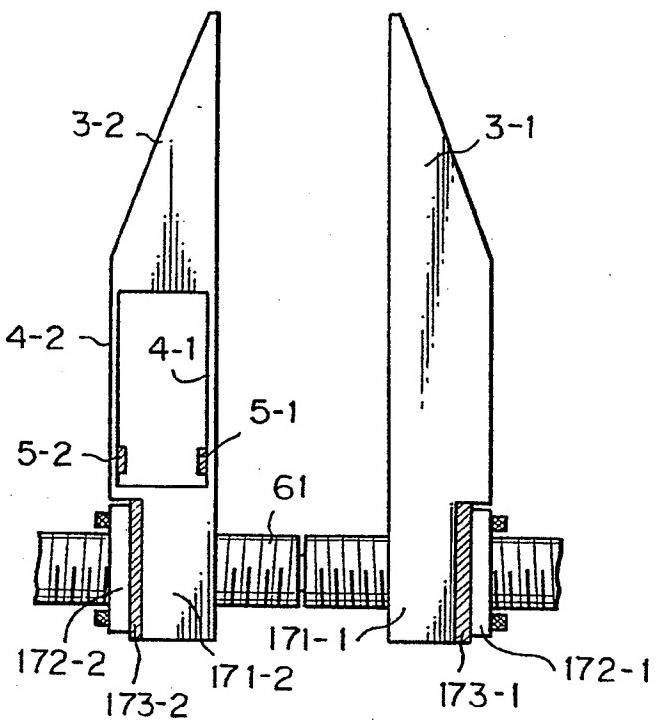
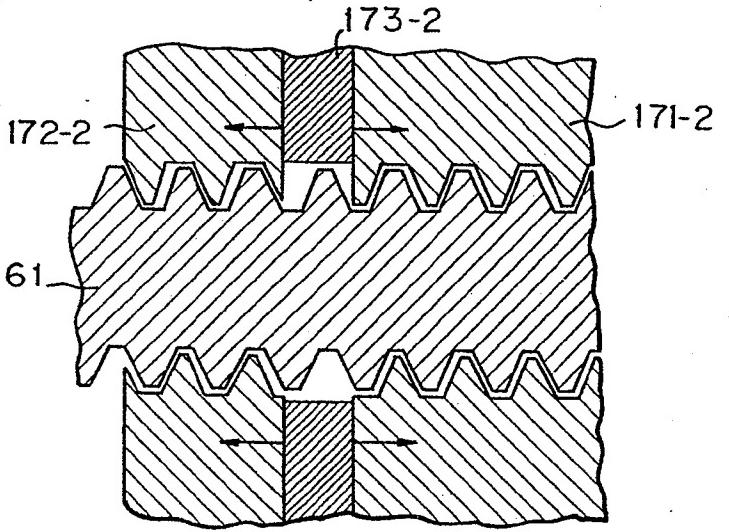


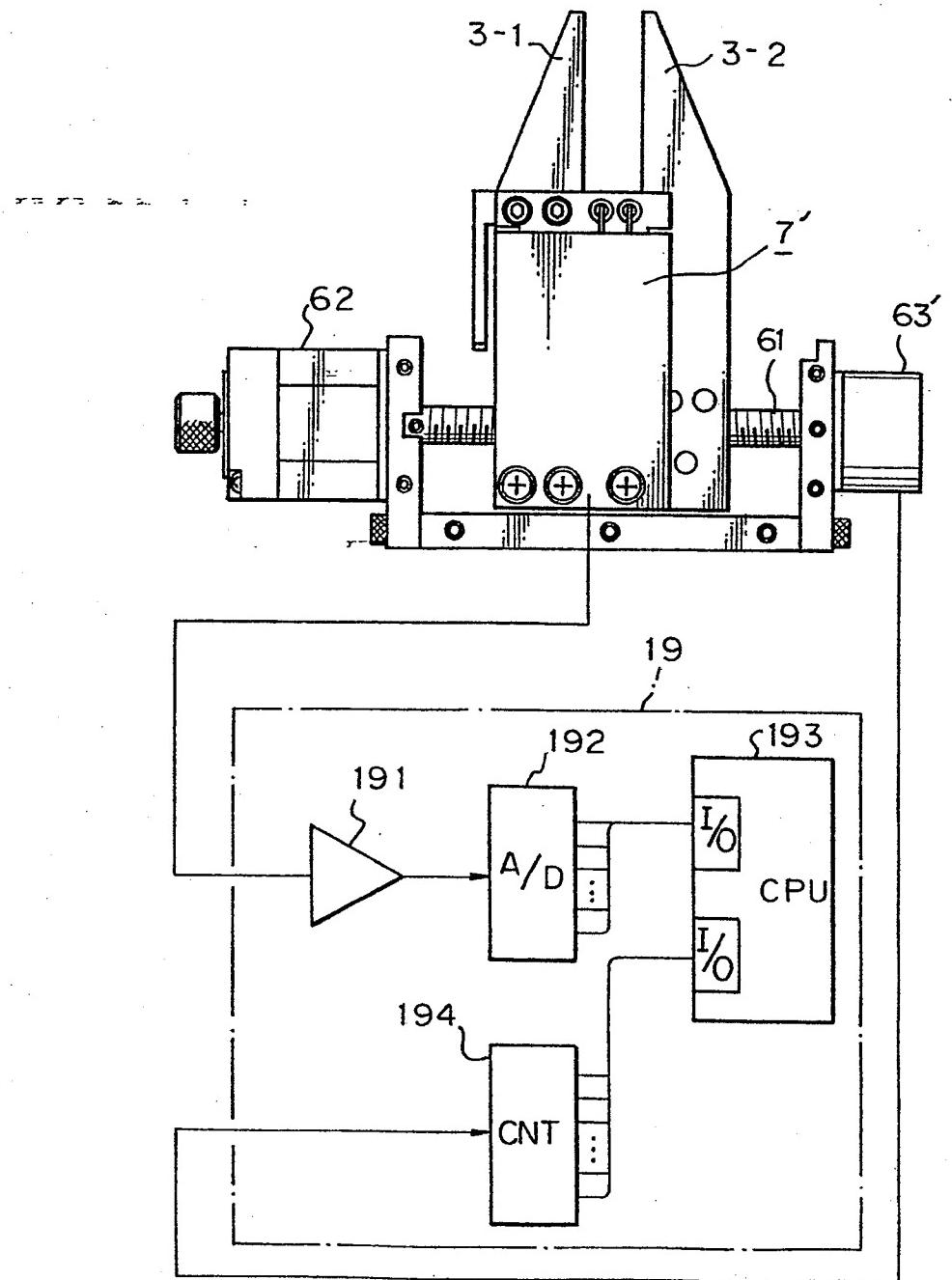
Fig. 18



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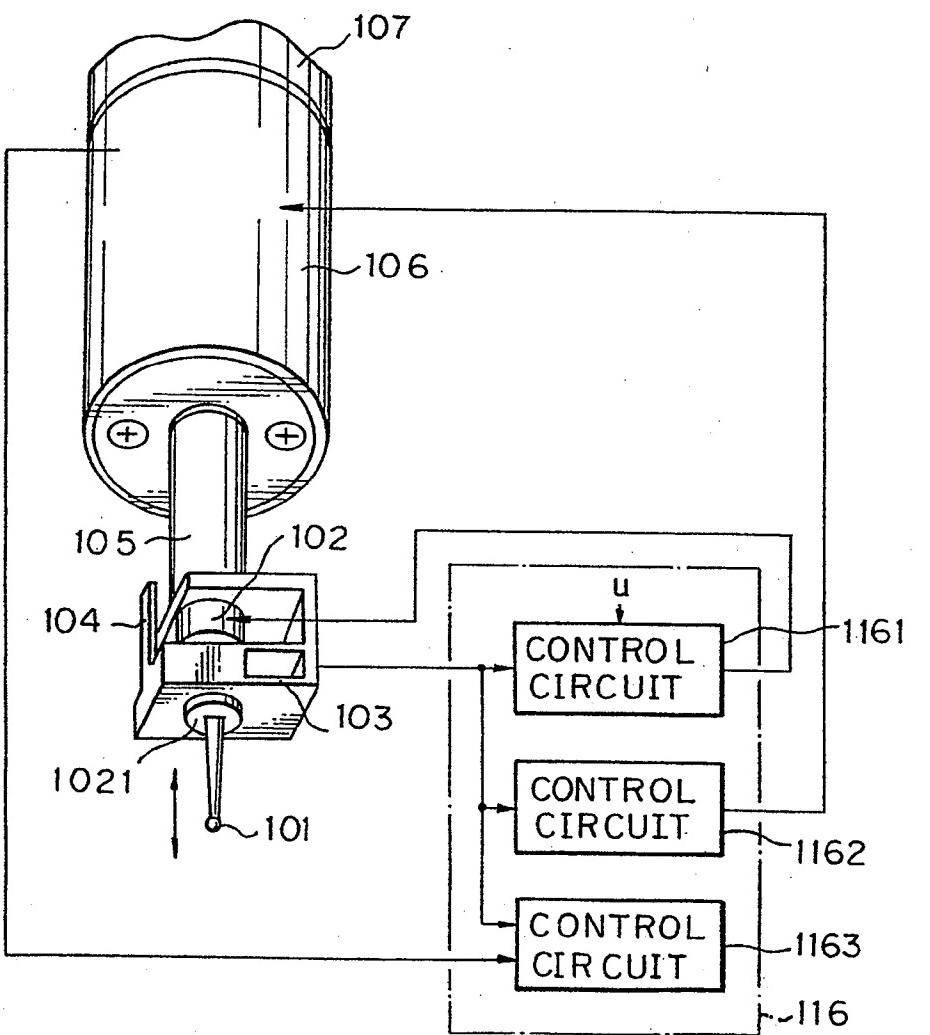
Fig. 19



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Fig. 20



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Fig. 21

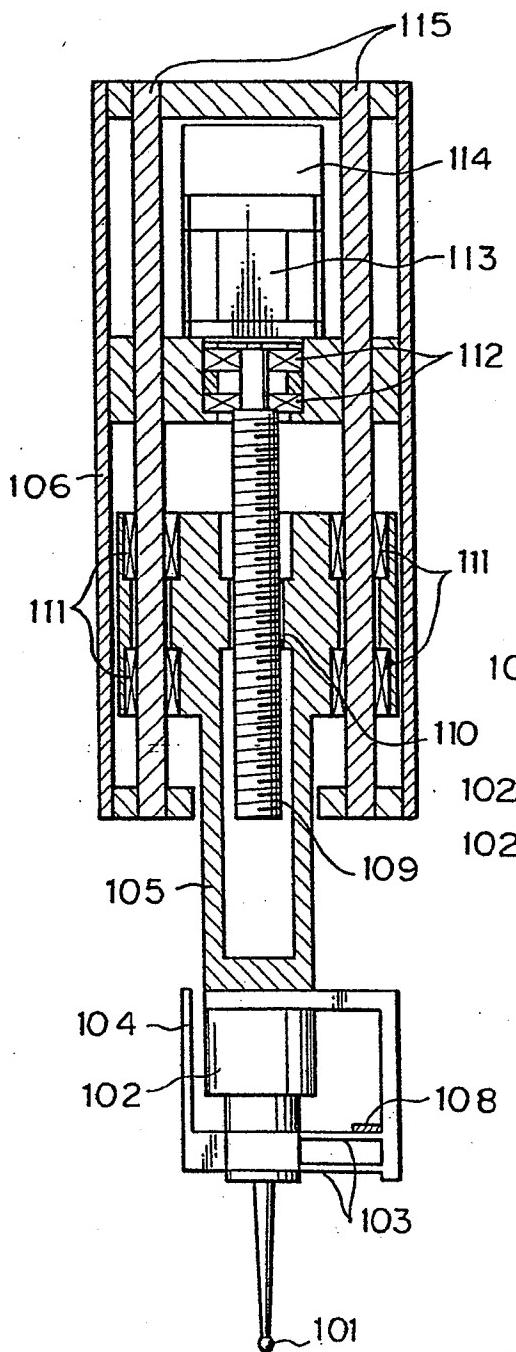
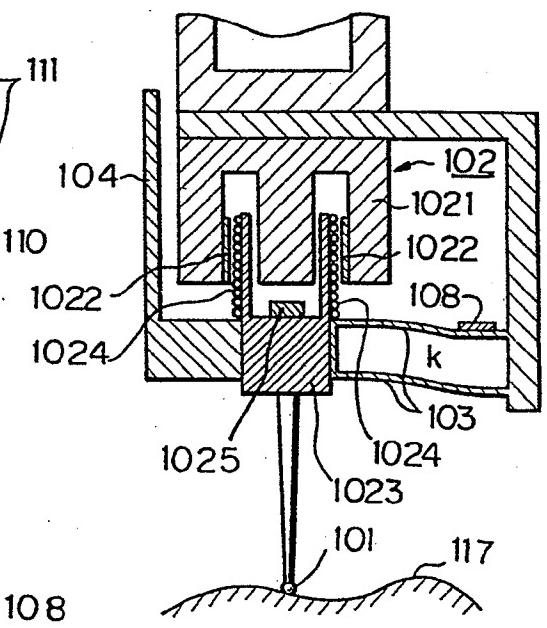


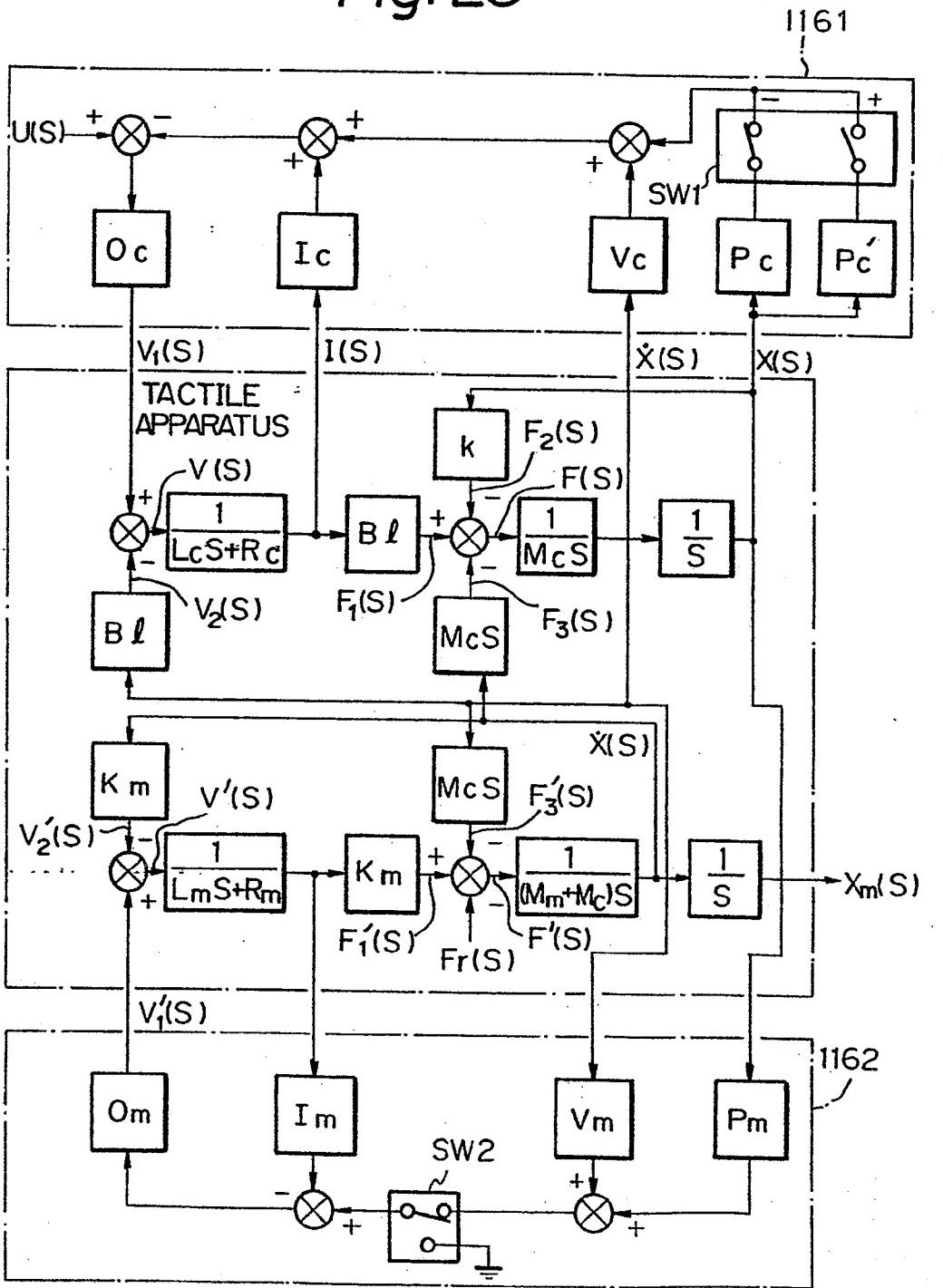
Fig. 22



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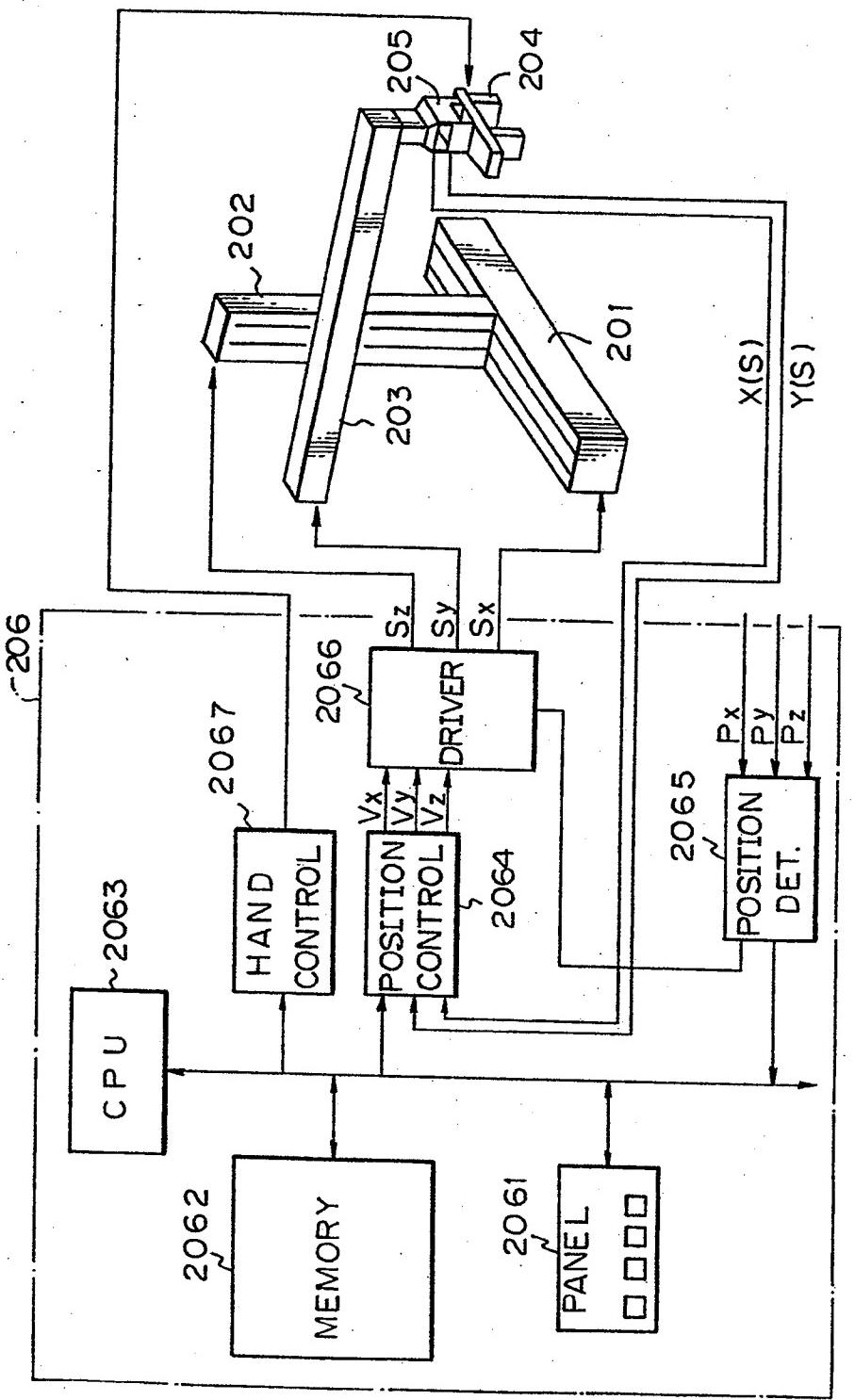
Fig. 23



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Fig. 24



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Fig. 25

